

Digital Signal Processing

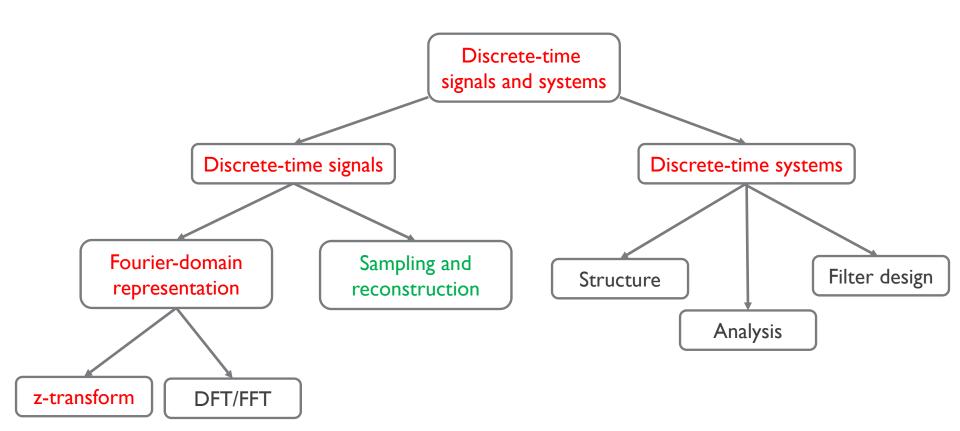
POSTECH

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Course at glance







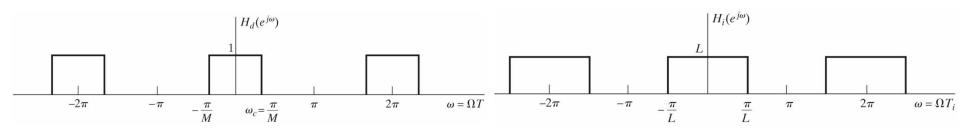
Multirate Signal Processing





Changing sampling rate possible

- Use downsampling/upsampling to reduce/increase the sampling rate
 - → Both systems need lowpass filters
- lacktriangle With large changing factors M and L, we need narrowband lowpass filters



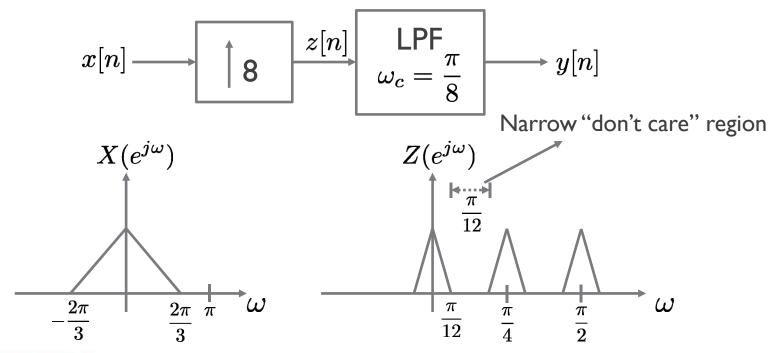
- Hard to implement narrowband lowpass filters with sharp cutoff frequency
 - → Requires "long" FIR filter
 - → Compare ideal lowpass filter and linear interpolation filter
- lacktriangle How to reduce the complexity of resampling for e.g., M=101 and L=100?





Example of multistage interpolation

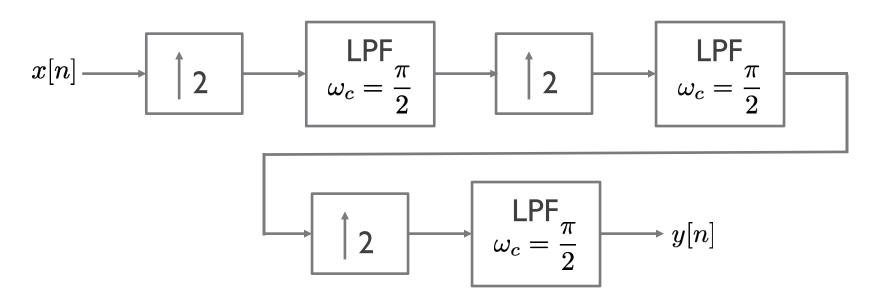
- Consider 4kHz bandwidth speech sampled at 12kHz
- Want to implement a system







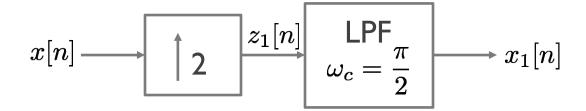
◆ Instead, consider implementing in 3 stages

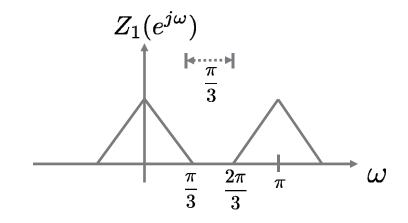






◆ Stage I

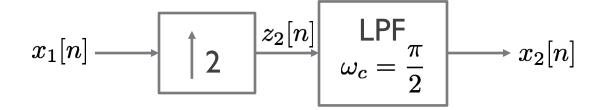


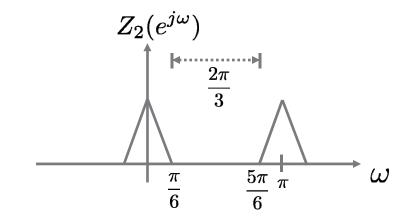






Stage 2

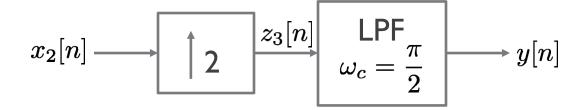


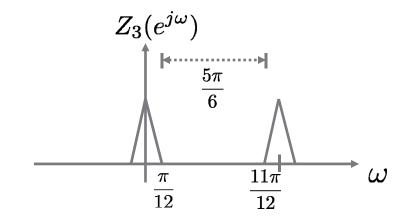






◆ Stage 3









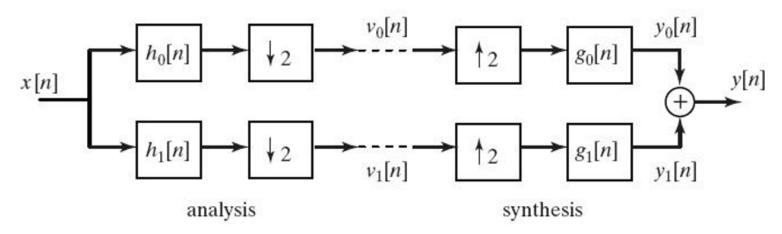
Multirate filter bank

- Split audio/speech signals into different frequency components
 - → Low, medium, high frequency components
 - → Process (quantize and/or storage) each frequency component separately
 - ★ Reconstruct the signal by synthesizing frequency components
- We can exploit downsampling/upsampling for multirate filter bank





Two-channel perfect reconstruction filter bank



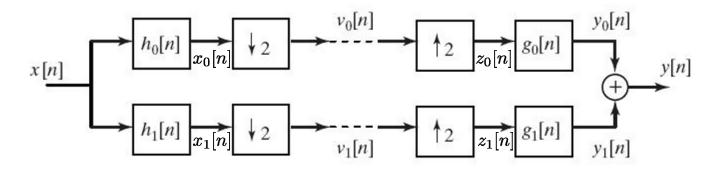
- Analysis part by downsampling / synthesis part by upsampling
- lacktriangle We want to have x[n]=y[n] without further processing on ----
- lacktriangle What are relationships among $h_0[n], h_1[n], g_0[n], g_1[n]$?
 - → Decomposition requires $h_0[n], h_1[n]$ to be lowpass and highpass filters $H_0(e^{j\omega})$: lowpass filter with passband $0 \le |\omega| \le \pi/2$



$$h_1[n] = e^{j\pi n} h_0[n] \stackrel{\mathcal{F}}{\longleftrightarrow} H_1(e^{j\omega}) = H_0(e^{j(\omega - \pi)})$$



Frequency-domain relationships



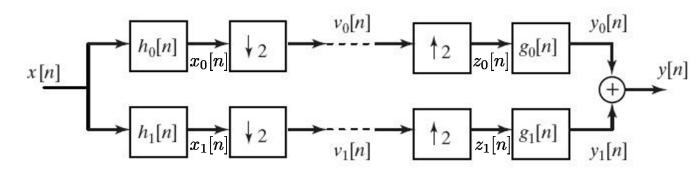
$$X_i(e^{j\omega}) = H_i(e^{j\omega})X(e^{j\omega})$$

$$V_{i}(e^{j\omega}) = \frac{1}{2} \left(X_{i}(e^{j\omega/2}) + X_{i}(e^{j(\omega-2\pi)/2}) \right)$$
$$= \frac{1}{2} \left(H_{i}(e^{j\omega/2}) X(e^{j\omega/2}) + H_{i}(e^{j(\omega-2\pi)/2}) X(e^{j(\omega-2\pi)/2}) \right)$$





Frequency-domain relationships



$$Z_i(e^{j\omega}) = V_i(e^{2j\omega})$$

$$= \frac{1}{2} \left(H_i(e^{j\omega}) X(e^{j\omega}) + H_i(e^{j(\omega-\pi)}) X(e^{j(\omega-\pi)}) \right)$$

$$Y(e^{j\omega}) = G_0(e^{j\omega})Z_0(e^{j\omega}) + G_1(e^{j\omega})Z_1(e^{j\omega})$$
 Potential aliasing distortion
$$= \frac{1}{2} \left(H_0(e^{j\omega})G_0(e^{j\omega}) + H_1(e^{j\omega})G_1(e^{j\omega}) \right) X(e^{j\omega})$$

$$+ \frac{1}{2} \left(H_0(e^{j(\omega-\pi)})G_0(e^{j\omega}) + H_1(e^{j(\omega-\pi)})G_1(e^{j\omega}) \right) X(e^{j(\omega-\pi)})$$



Ideal case

• With ideal filters that exactly split the band $0 \le |\omega| \le \pi$ without overlapping, it is easy to show that

$$(H_0(e^{j\omega})G_0(e^{j\omega}) + H_1(e^{j\omega})G_1(e^{j\omega}))) = 2$$
$$(H_0(e^{j(\omega-\pi)})G_0(e^{j\omega}) + H_1(e^{j(\omega-\pi)})G_1(e^{j\omega})) = 0$$

What about with non-ideal, practical filters?





Using practical filters

Alias cancellation condition

$$g_0[n] = 2h_0[n] \stackrel{\mathcal{F}}{\longleftrightarrow} G_0(e^{j\omega}) = 2H_0(e^{j\omega})$$
$$g_1[n] = -2h_1[n] \stackrel{\mathcal{F}}{\longleftrightarrow} G_1(e^{j\omega}) = -2H_0(e^{j(\omega-\pi)})$$

Combined with $h_1[n] = e^{j\pi n} h_0[n] \stackrel{\mathcal{F}}{\longleftrightarrow} H_1(e^{j\omega}) = H_0(e^{j(\omega-\pi)})$ $Y(e^{j\omega}) = |H_0^2(e^{j\omega}) - H_0^2(e^{j(\omega - \pi)})| X(e^{j\omega})$

$$lacktriangle$$
 Thus, perfect reconstruction (with possible delay of M samples) requires $H_0^2(e^{j\omega})-H_0^2(e^{j(\omega-\pi)})=e^{-j\omega M}$

 $lacktriangledown h_0[n]=c_0\delta[n-2n_0]+c_1\delta[n-2n_1-1]$ satisfies this condition $c_0c_1=1/4$ Arbitrary integer





Simple example

• Let
$$h_0[n] = \frac{1}{2}(\delta[n] + \delta[n-1]) \stackrel{\mathcal{F}}{\longleftrightarrow} H_0(e^{j\omega}) = \cos(\omega/2)e^{-j\omega/2}$$

$$\bullet H_0^2(e^{j\omega}) - H_0^2(e^{j(\omega - \pi)}) = \cos^2(\omega/2)e^{-j\omega} - \cos^2((\omega - \pi)/2)e^{-j(\omega - \pi)}$$

$$= \frac{1 + \cos\omega}{2}e^{-j\omega} + \frac{1 + \cos(\omega - \pi)}{2}e^{-j\omega}$$

$$= \frac{1 + \cos\omega}{2}e^{-j\omega} + \frac{1 - \cos\omega}{2}e^{-j\omega}$$

$$= e^{-j\omega}$$

$$= \cos^2\left(\frac{\omega}{2}\right) = \frac{1 + \cos\omega}{2}$$

- lacktriangle Therefore, y[n] = x[n-1]
- $h_0[n] = c_0 \delta[n-2n_0] + c_1 \delta[n-2n_1-1]$ is very crucial lowpass filter though





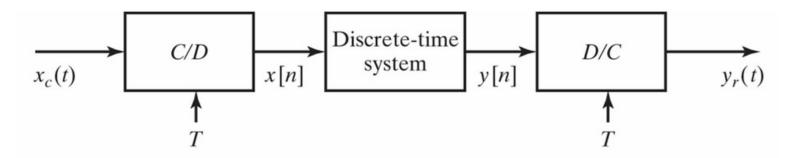
Digital Processing of Analog Signals





Ideal system

So far, we assumed ideal components for sampling and reconstruction



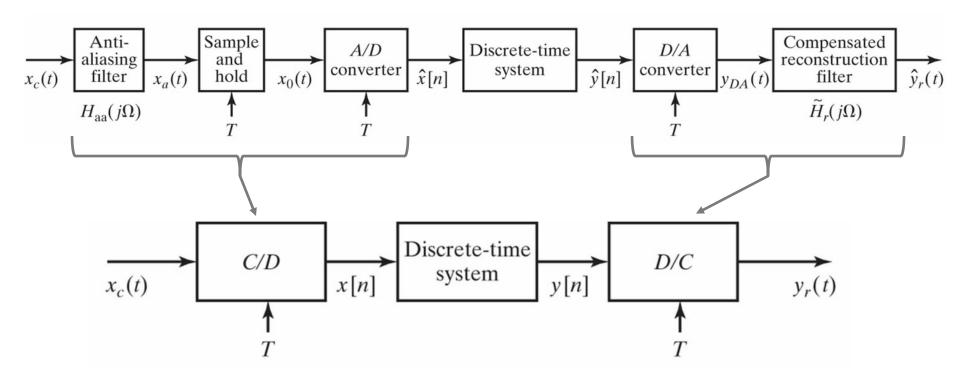
- In practice, they are not possible
 - → Input signal not band limited
 - → Impulse train
 - → Ideal lowpass filter
 - → Infinite precision
 - **→** Etc...





Practical system

General diagram of practical system







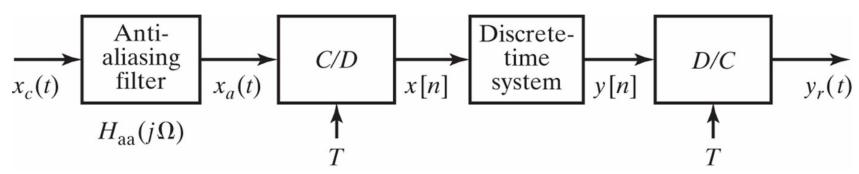
Antialiasing filter

- Input signal not bandlimited in general
 - + Even the signal is bandlimited, noise can have high frequency component
- Useful information may be contained only in low-frequencies
 - → Speech signal
 - Can have 3Hz~20kHz frequency range
 - 3~4kHz frequency range enough for intelligibility
- ◆ High-frequency components (unnecessary information or noise) can be aliased into the low-frequency band.
- Need analog lowpass filter before sampling to avoid aliasing





Ideal antialiasing filter



Frequency response of ideal antialiasing filter would be

$$H_{aa}(j\Omega) = \begin{cases} 1, & |\Omega| < \Omega_c \le \pi/T \\ 0, & |\Omega| \ge \Omega_c \end{cases}$$

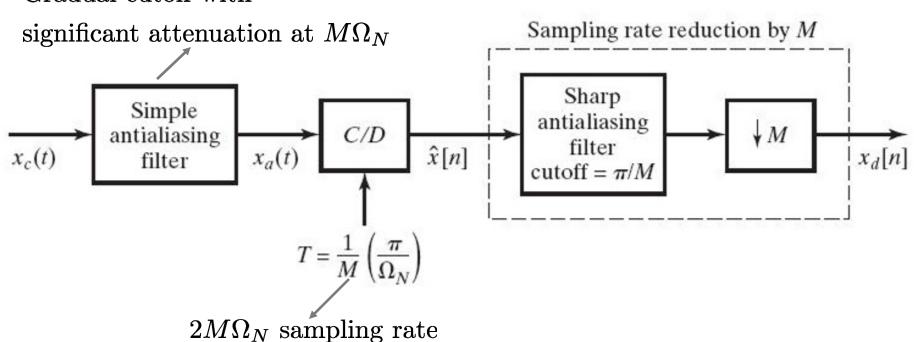
- This requires sharp cutoff frequency
 - → Can be implemented using active networks and integrated circuits
 - → Much harder & more expensive & less flexible than digital filters





Practical antialiasing filter design

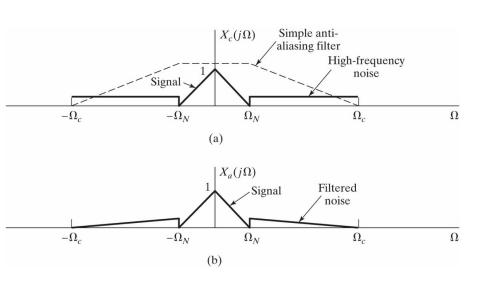
Gradual cutoff with

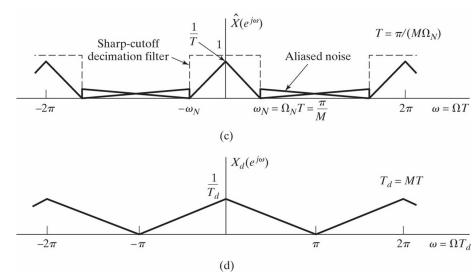






Frequency-domain illustration



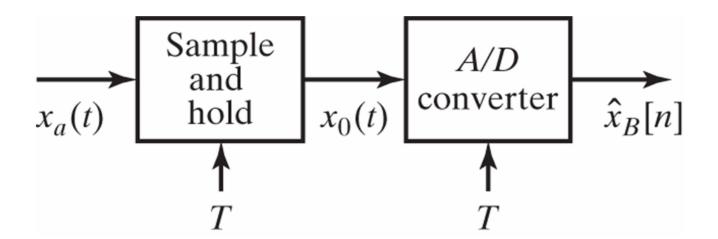






A/D conversion

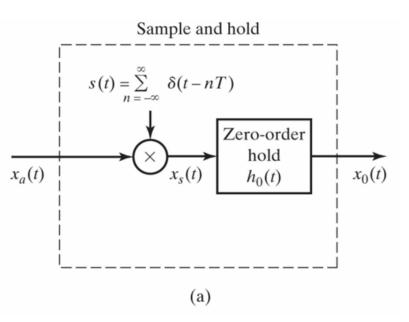
- Ideal C/D conversion not possible
 - + Impulse train, infinite precision of amplitude, ...
- Practical C/D conversion is A/D conversion



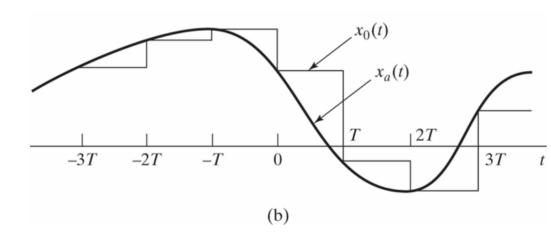




Sample-and-hold block



$$h_0(t) = \begin{cases} 1, & 0 < t < T, \\ 0, & \text{otherwise} \end{cases}$$



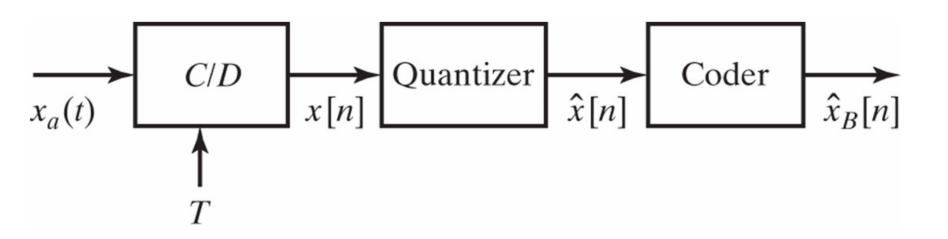
$$x_0(t) = \sum_{n = -\infty}^{\infty} x[n]h_0(t - nT)$$

$$= h_0(t) * \sum_{n=-\infty}^{\infty} x_a(nT)\delta(t - nT)$$





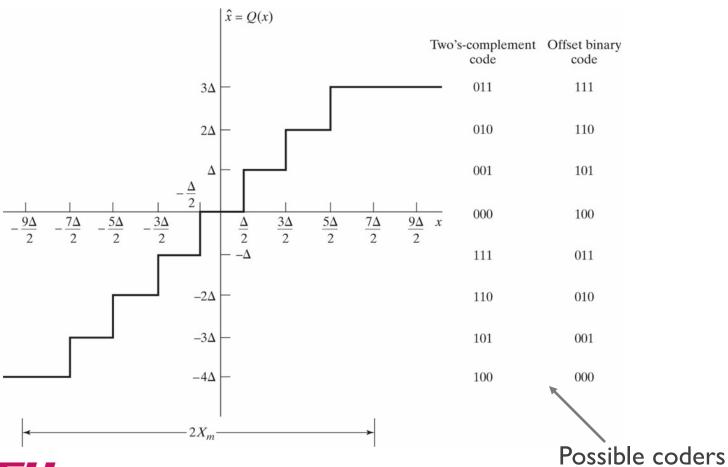
Conceptual illustration of A/D







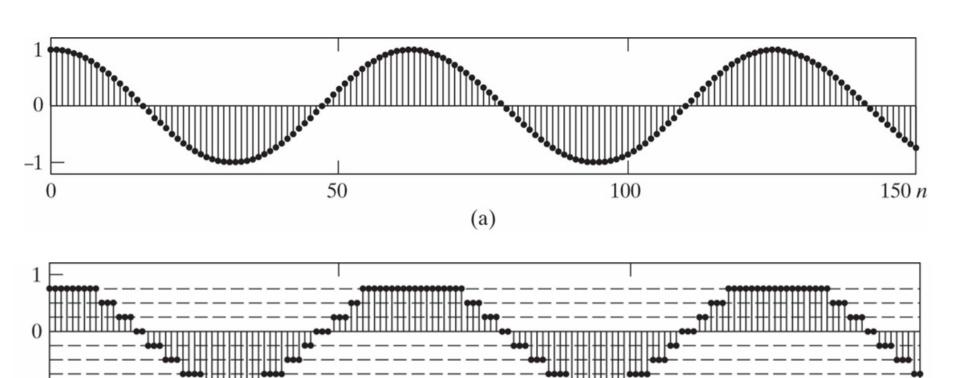
Quantizer and coder







Example



(b)

50

100

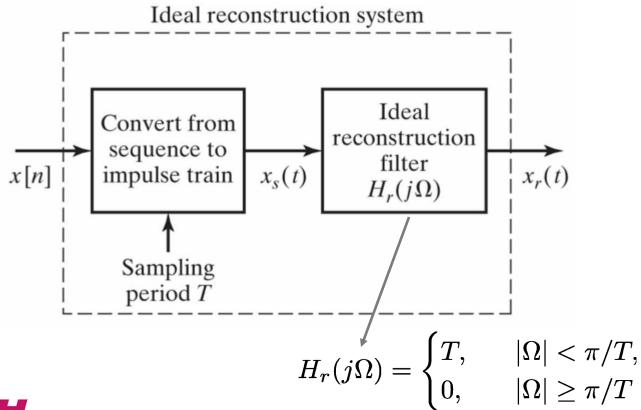


150 n



D/A conversion

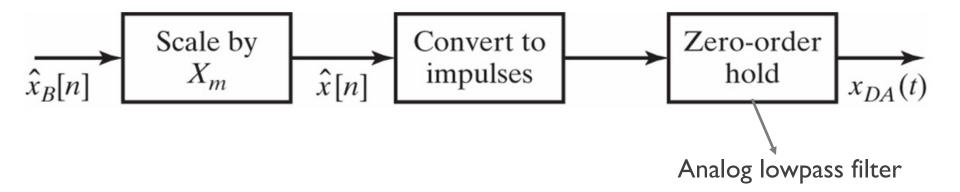
Ideal D/C conversion







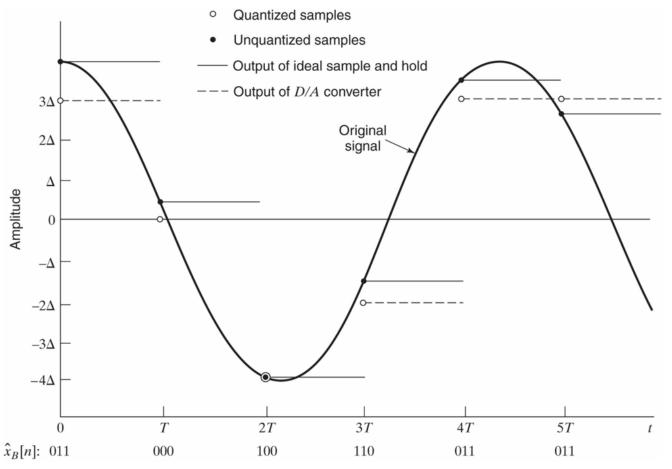
Practical D/A conversion







Time-domain illustration of D/A conversion







Issue

◆ The frequency response of the zero-order-hold filter

$$H_0(j\Omega) = \frac{2\sin(\Omega T/2)}{\Omega}e^{-j\Omega T/2}$$

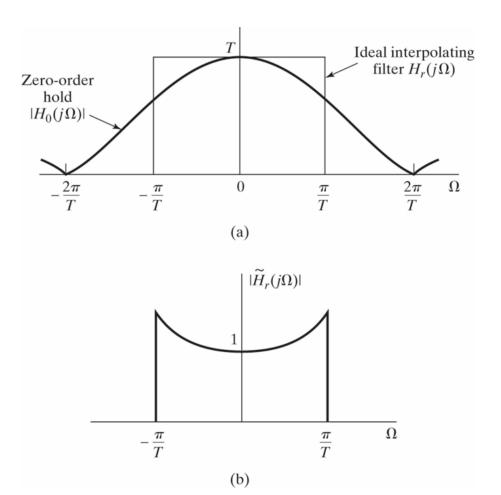
Need a compensated reconstruction filter

$$ilde{H}_r(j\Omega)=rac{H_r(j\Omega)}{H_0(j\Omega)}$$
 Ideal lowpass filter





Frequency-domain illustration







Homework

- Problems in textbook: 4.23, 4.25, 4.28, 4.31, 4.34
 - → Solution uploaded on the webpage

