

# Optoelectronics (광전자공학)

## Lecture 9. Surface Emitting Lasers

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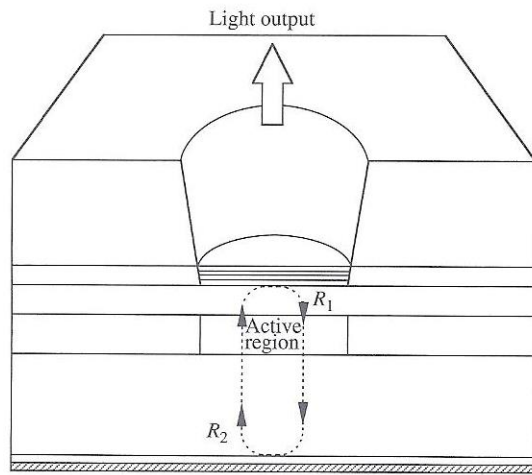
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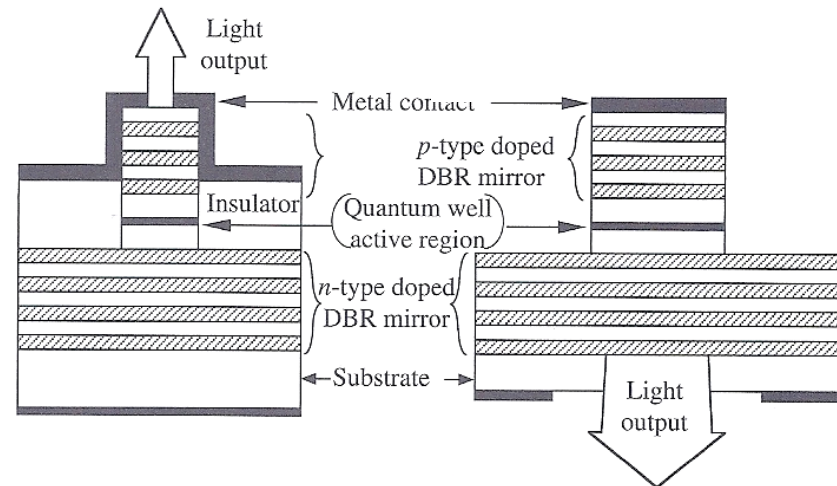
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# Surface Emitting Lasers

## ■ Vertical-cavity surface-emitting laser (VCSEL)



Schematic diagram of a surface emitting laser



Front and back surface-emitting lasers

### Advantages

- ✓ Ease of coupling to optical fibers( ∵ circular geometry)
- ✓ Direct wafer scale probing, two-dimensional laser array( ∵ vertical emission from the top or bottom of substrate)
- ✓ Ultralow threshold operation, single-frequency operation( ∵ small cavity volume)
- ✓ Fabrication process without wafer lapping, device cleaving and dicing, facet coating, wire bonding

# Surface Emitting Lasers

## ■ Brief VCSEL history

Year	Event	Material	Wavelength
1977	First suggestion	AlGaAs/GaAs	0.85 $\mu\text{m}$
1979	First demonstration	InGaAsP/InP	1.3 $\mu\text{m}$
1984	Semiconductor DBR	InGaAsP/InP	1.3 $\mu\text{m}$
1986	Semiconductor DBR	AlGaAs/GaAs	0.85 $\mu\text{m}$
1986	6mA threshold at room temperature	AlGaAs/GaAs	0.85 $\mu\text{m}$
1988	First room temperature(RT) CW	AlGaAs/GaAs	0.85 $\mu\text{m}$
1989	2mA threshold quantum well device	InGaAs/GaAs	0.98 $\mu\text{m}$
1989	Sub-mA threshold device	AlGaAs/GaAs	0.98 $\mu\text{m}$
1991	First RT operation of deep red	InGaAsP/InP	0.78 $\mu\text{m}$
1993	First RT CW long wavelength	InGaAlP/GaAs	1.3 $\mu\text{m}$
1993	First RT operation of red color	InGaAs/GaAs	0.67 $\mu\text{m}$
1995	Oxidation of AlAs and sub-200 $\mu\text{A}$ threshold	AlGaAs/GaAs	0.98 $\mu\text{m}$
1996	10 <sup>7</sup> hours of life time	AlGaAs/GaAs	0.85 $\mu\text{m}$
1996	> 200 mA CW output	InGaAs/GaAs	0.98 $\mu\text{m}$
1996	> 50% power conversion efficiency	InGaAs/GaAs	0.98 $\mu\text{m}$
1998	Optically pumped blue color	InGaN/GaN	0.4 $\mu\text{m}$

# Surface Emitting Lasers

## ■ First suggestion



Sketch of VCSEL conceived in 1977



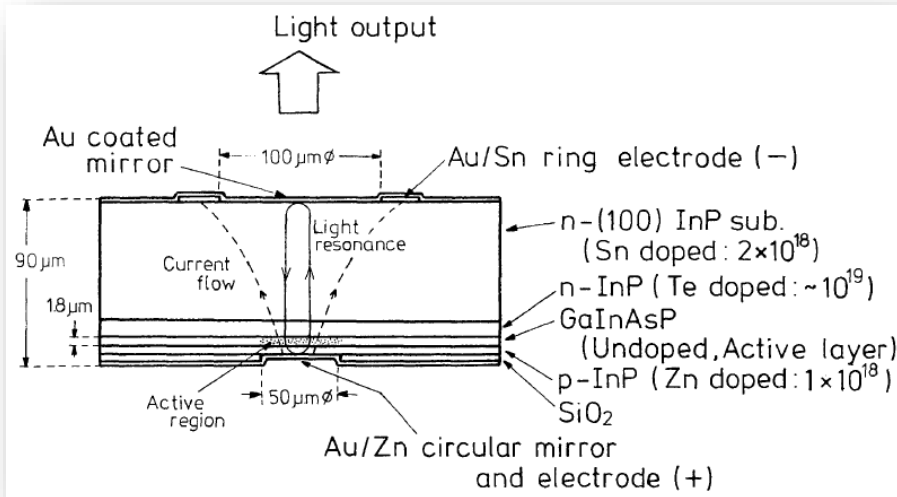
Prof. Kenichi Iga

- ✓ This type of laser was first proposed by Prof. Kenichi Iga in 1977 at the Tokyo Institute of Technology as an alternative device design that could be packaged in a manner similar to that of a light-emitting diode (LED) and yet could be very simply and efficiently coupled to a fiber.

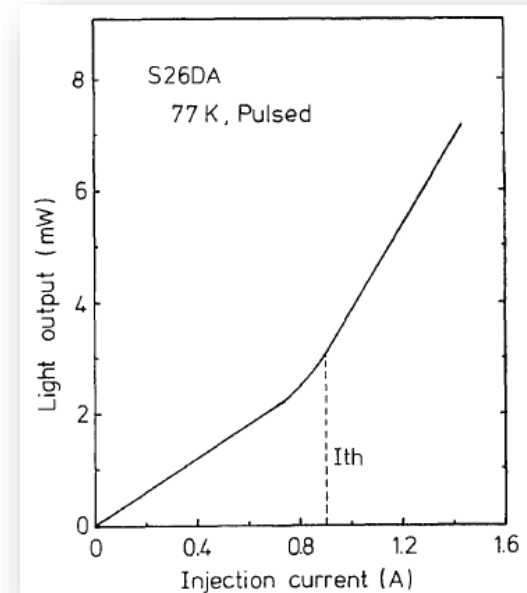
K. Iga, "Vertical-cavity surface-emitting laser: It's conception and evolution," *J. J. Appl. Phys.* 47, 1-10 (2008).

# Surface Emitting Lasers

## ■ First demonstration



Schematic structure of InGaAsP/InP surface emitting injection laser



Light output vs. injection current characteristic

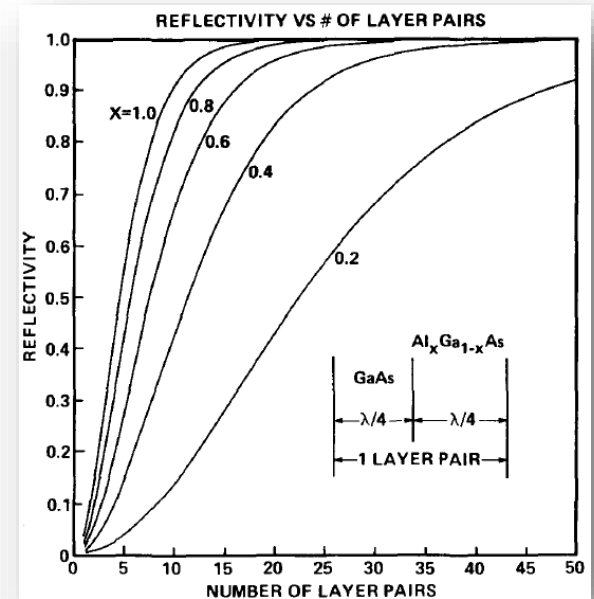
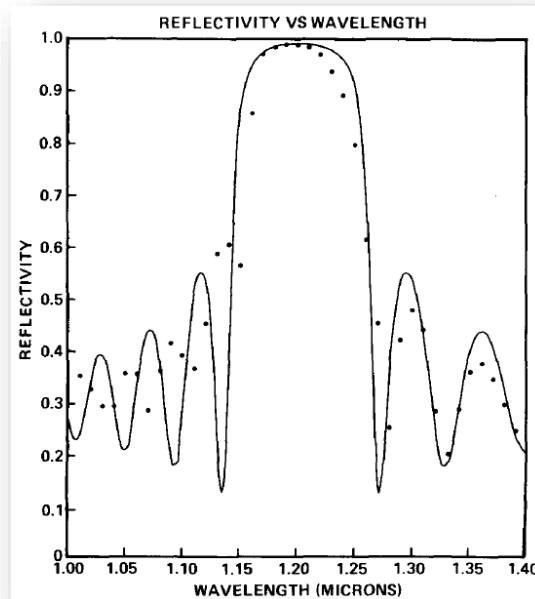
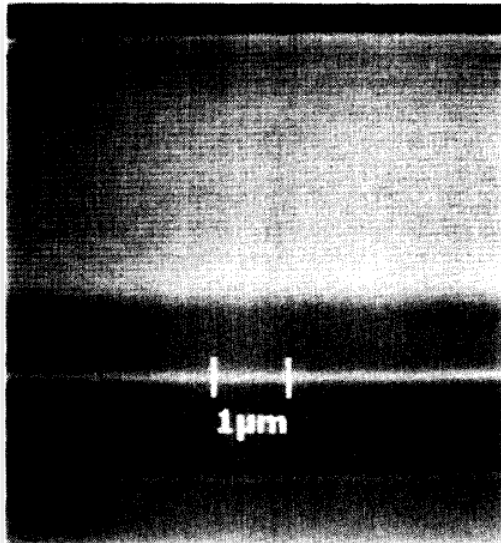
✓ n-type InP layer, undoped InGaAsP active layer, p-type InP layer were grown sequentially on a (100) n-type InP substrate using *liquid phase epitaxy*(LPE).

✓ Threshold current was **900 mA at 77 K** and light output of **several mW** was obtained.

H. Soda, K. Iga, O. Kitahara, and Y. Suematsu, "GaInAsP/InP surface emitting injection lasers," *J. J. Appl. Phys.* 18, 2329-2330 (1979).

# Surface Emitting Lasers

## ■ First GaAs/AlGaAs DBR mirror

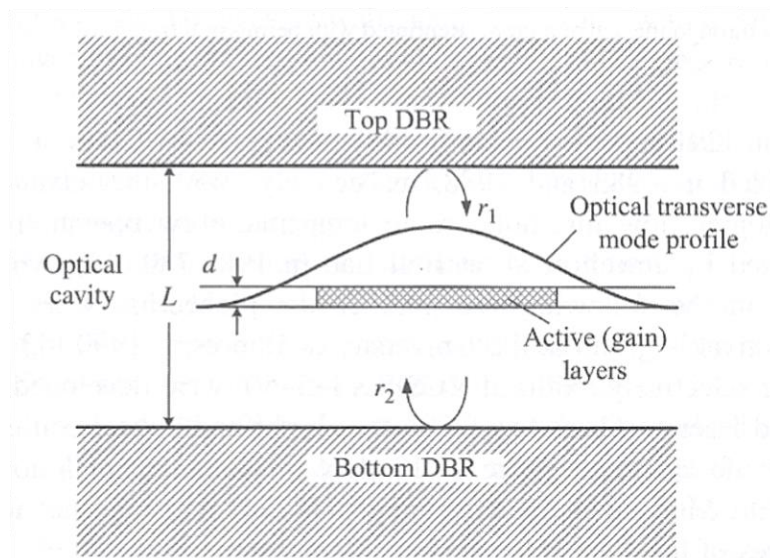


✓ 40 layers of alternating GaAs/Al<sub>0.6</sub>Ga<sub>0.4</sub>As epitaxially grow on GaAs substrates using *metal organic chemical vapor deposition(MOCVD)*.

# Surface Emitting Lasers

## ■ Lasing condition

The lasing condition of a VCSEL is round-trip resonance condition of a vertical Fabry-Perot cavity



Round-trip propagation condition for the lasing oscillation of a mode in a VCSEL cavity

$$r_1 r_2 e^{i2\beta L} = 1 \quad \text{Eq. (11.2.1a)}$$

Complex propagation constant

$$\beta = \beta_c + i \frac{(\alpha - \Gamma g)}{2} \quad \text{Eq. (11.2.1b)}$$

Real part

$$\beta_c = \frac{2\pi}{\lambda} n = \frac{\omega}{c} n$$

Imaginary part

$\alpha$ : absorption coefficient

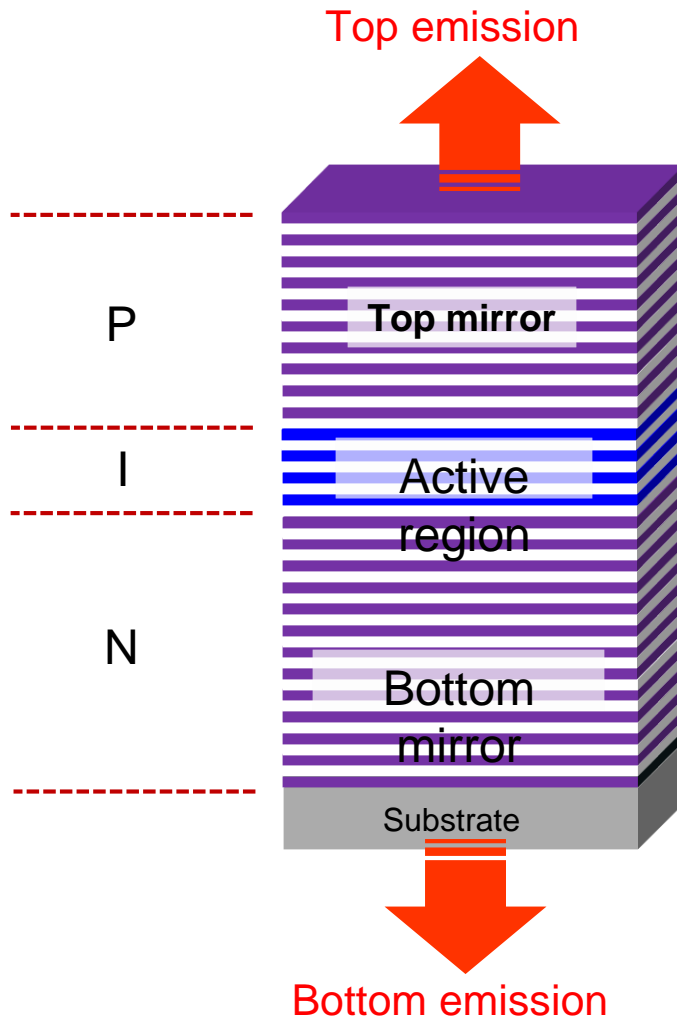
$\Gamma g$ : threshold gain

$$r_1 = |r_1| e^{i\phi_1} \quad r_2 = |r_2| e^{i\phi_2}$$

Complex reflection coefficients for the DBR mirrors at the top & bottom

# Surface Emitting Lasers

## ■ Basic VCSEL structure



### ➤ *Mirror design issue*

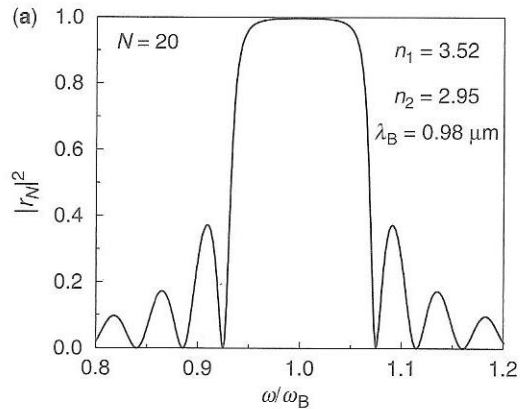
- ✓ High mirror reflectivity
- ✓ High reflective index contract
- ✓ Compatible with the quantum layer
- ✓ Low series resistance
- ✓ Low optical absorption loss
- ✓ DBR (distributed Bragg reflector) & metal

### ➤ *Active region design issue*

- ✓ High optical gain
- ✓ Low threshold current
- ✓ High coupling efficiency between gain and optical field
- ✓  $n\lambda/2$  (optical thickness)  
: spacer+gain layer(quantum wells)

# Surface Emitting Lasers

## ■ Plane wave reflection from a distributed-Bragg reflector



For  $(2N+1)$  layers, the power reflectivity becomes

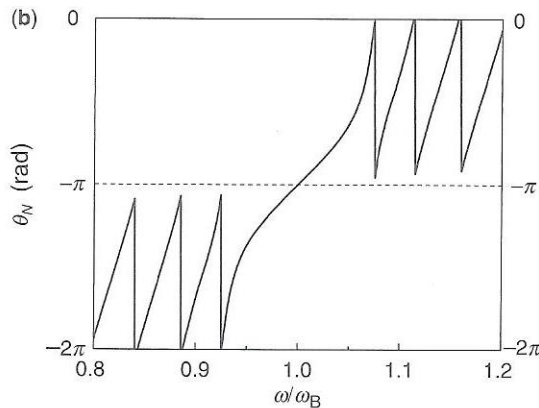
$$|r_N|^2 = \frac{R_1}{R_1 + (1 - R_1) \left( \frac{\sin \alpha}{\sin(N\alpha)} \right)^2}$$

Eq. (5.9.44)

N approaches a large number,

$$\left( \frac{\sin \alpha}{\sin(N\alpha)} \right)^2 \rightarrow e^{(-2(N-1)\alpha)} \rightarrow 0$$

$$|r_N|^2 \rightarrow 1$$



$$r_N = \frac{m_{21}}{m_{11}} e^{i2\phi_1} = |r_N| e^{i\theta_N}$$

(a) The power reflectivity of a DBR structure is plotted as a function of wavelength near the stop band wavelength.

(b) The phase of the reflection coefficient.

# Surface Emitting Lasers

- Special case right at resonance  $\lambda=\lambda_B$

*Reflection coefficient at resonance wavelength,*

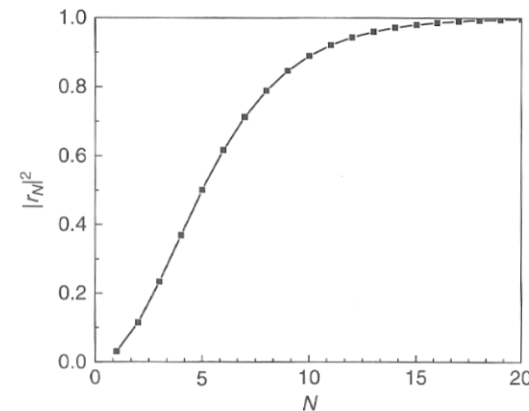
$$r_N = \frac{b^N \left( \frac{n_t}{n_1} \right) - a^N \left( \frac{n_1}{n_0} \right)}{b^N \left( \frac{n_t}{n_1} \right) + a^N \left( \frac{n_1}{n_0} \right)} = \frac{\left( \frac{n_2}{n_1} \right)^{2N} - \left( \frac{n_1^2}{n_0 n_t} \right)}{\left( \frac{n_2}{n_1} \right)^{2N} + \left( \frac{n_1^2}{n_0 n_t} \right)}$$

*Eq. (5.9.49)*

$$r_N \rightarrow \begin{cases} +1 & \text{if } n_2 > n_1 \\ -1 & \text{if } n_2 < n_1 \\ 0 & \text{if } \left( \frac{n_2}{n_1} \right)^{2N} = \frac{n_1^2}{n_0 n_t} \end{cases} \quad \begin{matrix} \text{Eq. (5.9.50)} \\ \\ \text{Eq. (5.9.51)} \end{matrix}$$

Assuming  $n_1(\text{GaAs})=3.52$  and  $n_2(\text{AlAs})=2.95$  at  $\lambda_B=0.98\mu\text{m}$   
 $n_0=n_t=n_1(\text{GaAs})=3.52$

$$|r_N|^2 = \left| \frac{\left( \frac{n_2}{n_1} \right)^{2N} - 1}{\left( \frac{n_2}{n_1} \right)^{2N} + 1} \right|^2 \quad \text{Eq. (5.9.52)}$$

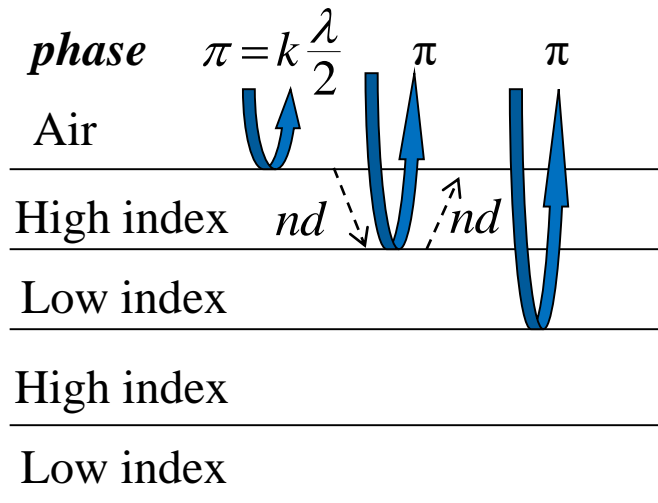


$|r_N|^2$  approaches unity quickly as N is above 10

# Surface Emitting Lasers

## ■ Design issues for distributed Bragg reflectors (DBRs)

- ✓ DBR is formed from multiple layers of alternating materials with varying refractive index to get the high reflection like mirror.
- ✓ from each individual interface added exactly **in phase** with the reflection from every other interface



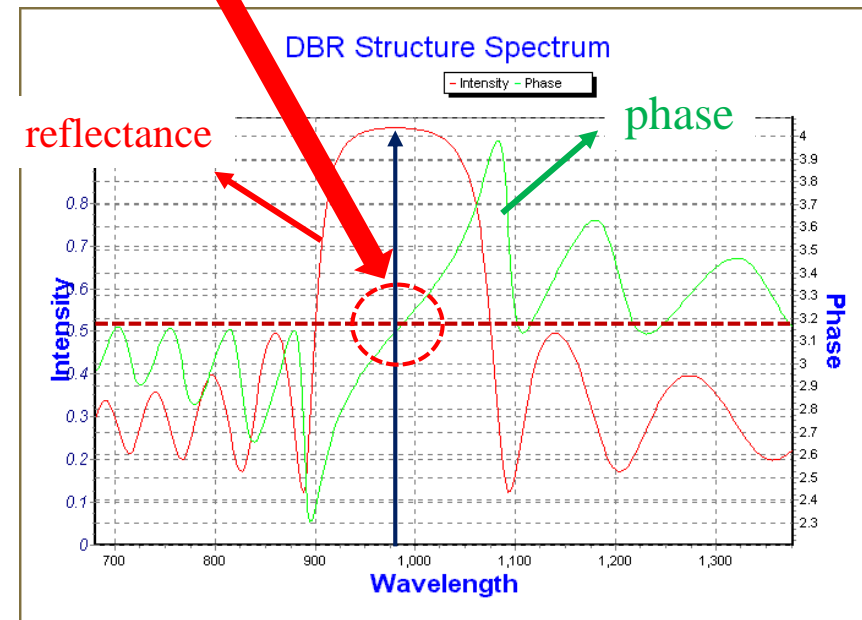
### In-phase condition

$$2nd = m\lambda + \frac{\lambda}{2}$$

$$\therefore d = \frac{\lambda}{4n}(2m+1)$$

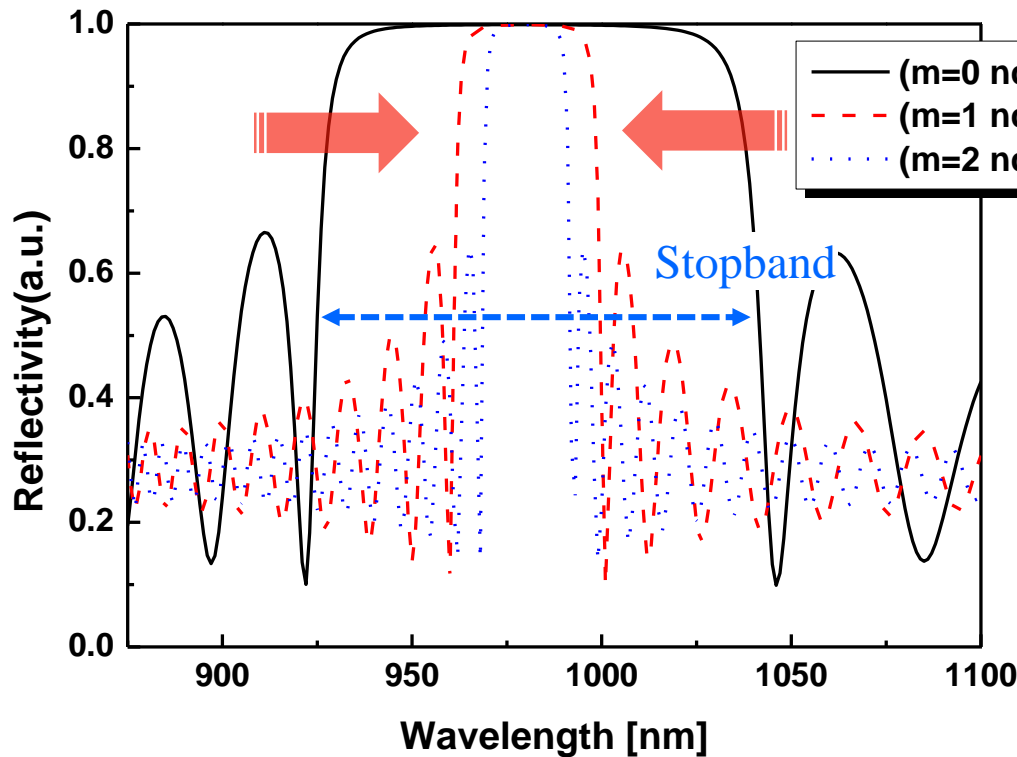
$n$  : refractive index  
 $d$  : thickness of each layer  
 $m$  : integer  
 $\lambda$  : wavelength in vacuum

- ✓ Thickness of DBR layers must satisfy **Bragg condition** at target wavelength !



# Surface Emitting Lasers

## ■ Design issues for distributed Bragg reflectors (DBRs)



*Bragg condition*

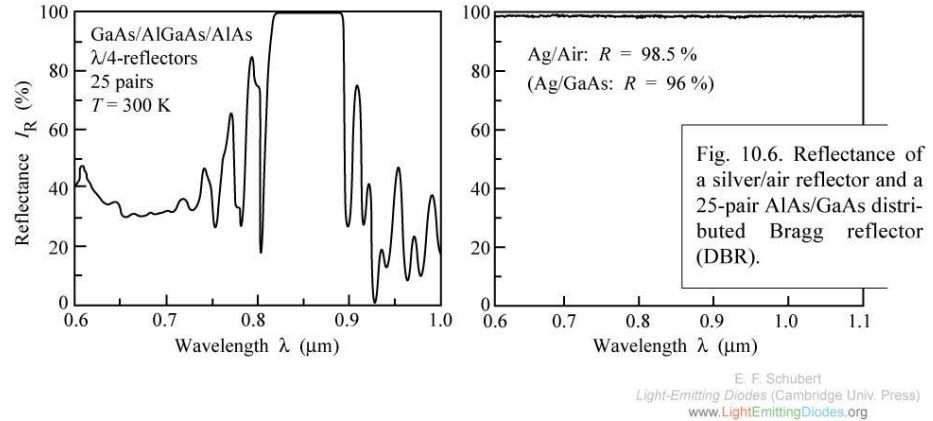
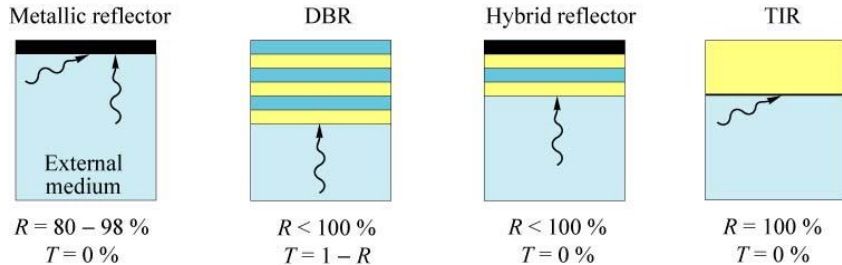
$$d = \frac{\lambda}{4n} (2m+1)$$

- ✓ Thicker thickness of DBR layers cause a decrease of stopband of reflectance.
- ✓ Small stopband design increase experimental difficulties and decrease error tolerance.

$\lambda = 980\text{nm}$   
GaAs( $m\lambda/4n$ ) / AlAs( $m\lambda/4n$ )-20pair

# Surface Emitting Lasers

## ■ Different types of reflectors



- ✓ Metallic reflector and hybrid reflectors are absorbing and cannot be used as light-exit reflectors ( $T = 0 \%$ ).
- ✓ Total internal reflectors(TIR) require that the angle of incidence be shallow in order to achieve high reflectivity.
- ✓ Distributed Bragg reflector(DBR) display narrow band of high reflectivity.

$$R_{DBR} = |r_N|^2 = \left| \frac{\left(\frac{n_2}{n_1}\right)^{2N} - 1}{\left(\frac{n_2}{n_1}\right)^{2N} + 1} \right|^2 \quad \text{Eq. (5.9.52)}$$

$$\Delta\lambda_{stopband} = \frac{2\lambda_{Bragg}(n_2 - n_1)}{\pi n_{eff}}$$

$$n_{eff} = 2 \left( \frac{1}{n_1} + \frac{1}{n_2} \right)^{-1}$$

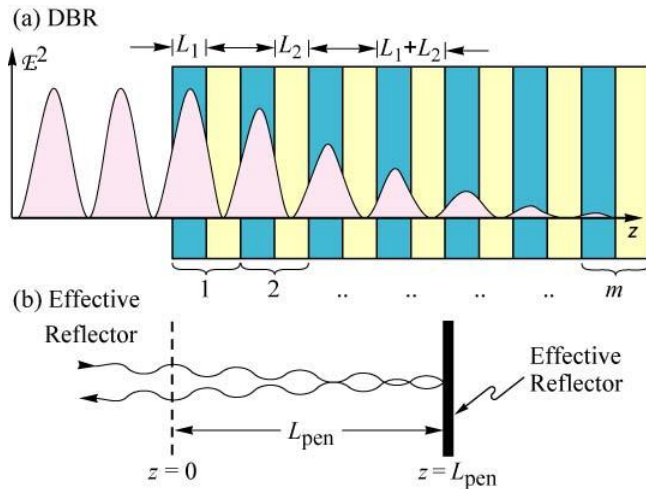
$n_2$ : high refractive index  
 $n_1$ : low refractive index

E. F. Schubert, "Light-Emitting diodes," Cambridge university press (2006).

L. A. Coldren et al., "Vertical-cavity surface-emitting lasers: Design, fabrication, characterization, and applications," Cambridge university press (1999).

# Surface Emitting Lasers

## Effective mirror model



< Illustration of the DBR penetration depth >

Knowing that the reflection phase is zero at the Bragg wavelength( $\beta_0$ ), we can express reflection coefficient (r) as

$$r_{DBR}|_{z=0} = |r_{DBR}|e^{i\varphi} = |r_{DBR}|e^{2i\left(\frac{2\pi}{\lambda}\right)L_{pen}}$$

$$r_{DBR} = |r_{DBR}|e^{i\varphi} = |r_{DBR}|e^{-2i(\beta-\beta_0)L_{pen}}$$

(within the linear region)

The incident and reflected wave amplitudes each experience a phase shift of  $\beta L_{pen}$  in traversing the distance to the effective mirror and back.

$$\beta: \text{average propagation constant} \quad \frac{1}{\beta} = \frac{1}{2} \left( \frac{1}{\beta_1} + \frac{1}{\beta_2} \right)$$

Expanding the simulated DBR reflection phase in a Taylor series about the Bragg wavelength

$$\begin{aligned} \varphi &= \varphi_0 + (\beta - \beta_0) \frac{\partial \varphi}{\partial \beta} + \frac{(\beta - \beta_0)^2}{2} \frac{\partial^2 \varphi}{\partial \beta^2} + \dots \\ &= -2(\beta - \beta_0)L_{pen} \end{aligned}$$

$$L_{pen} = -\frac{1}{2} \frac{\partial \varphi}{\partial \beta} \quad \text{Penetration depth}$$

✓ Effective cavity length

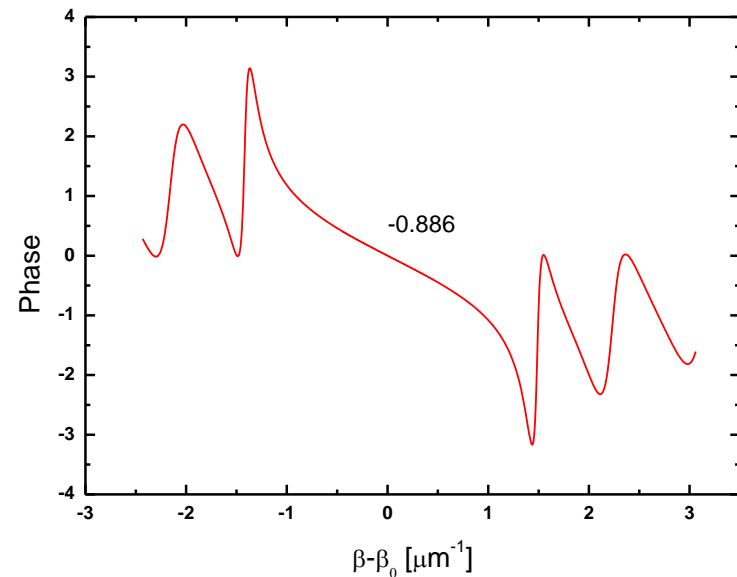
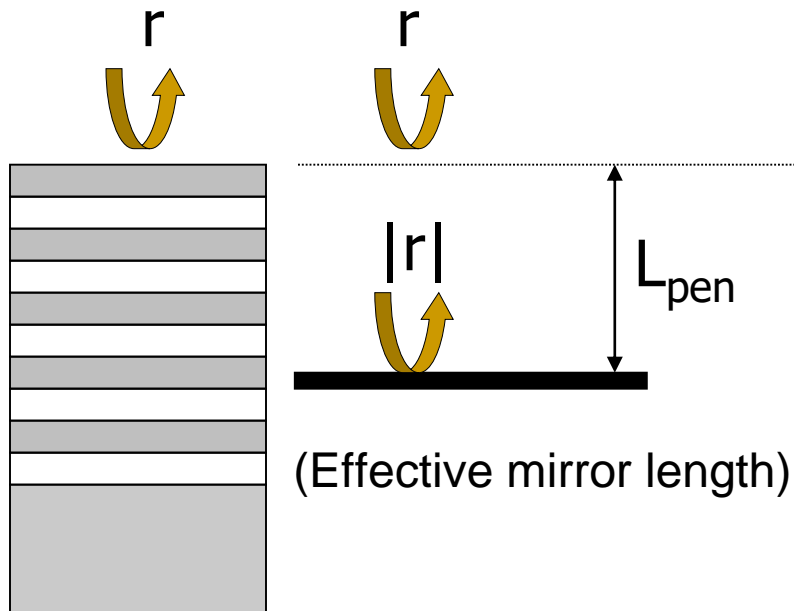


$$L_{eff} = L_{cavity} + L_{pen,topDBR} + L_{pen,bot.DBR}$$

# Surface Emitting Lasers

## ■ Effective mirror model

Phase varies relatively linearly near the reflection maximum. Such a reflection can be well approximated by a discrete mirror reflection equal to the magnitude of the reflection but placed a distance  $L_{\text{eff}}$  away.



$$L_{\text{pen}} = -\frac{1}{2} \frac{\partial \varphi}{\partial \beta} = 0.443 \mu\text{m}$$

# Surface Emitting Lasers

## ■ Design issues for active region I- Phase condition

$$\beta_c = \frac{2\pi}{\lambda} n$$

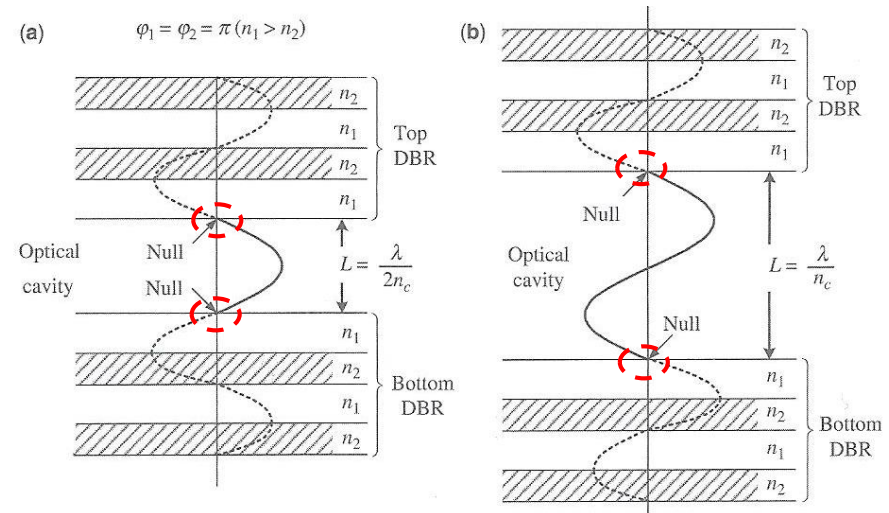
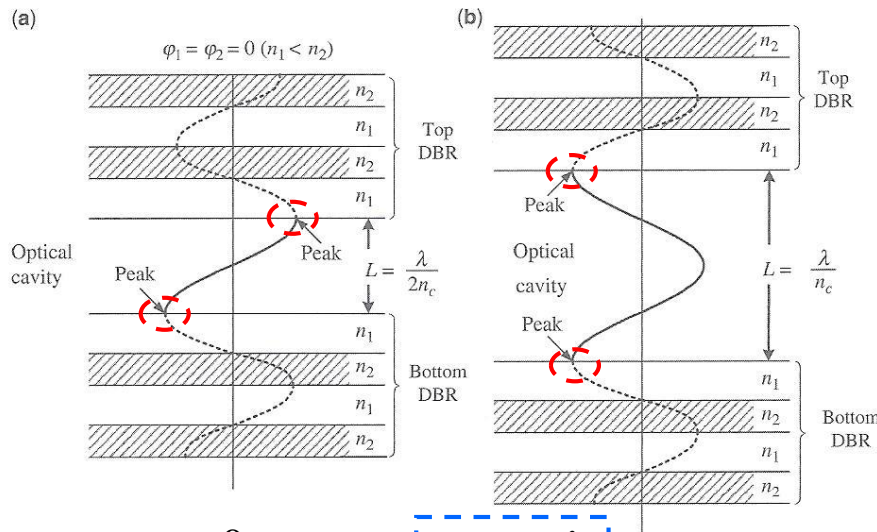
The phase condition of a VCSEL is

$$\varphi_1 + \varphi_2 + 2\beta_c L = 2m\pi$$

Eq. (11.2.3)

*lasing condition*

$$\left| r_1 \right| \left| r_2 \right| e^{i(\varphi_1 + \varphi_2 + 2\beta L)} = 1$$



$$\varphi_1 = \varphi_2 = 0$$

$$(n_1 < n_2)$$

$$L = m \frac{\lambda}{2n}$$

$$\varphi_1 = \varphi_2 = \pi$$

$$(n_1 > n_2)$$

$$L = (m-1) \frac{\lambda}{2n}$$

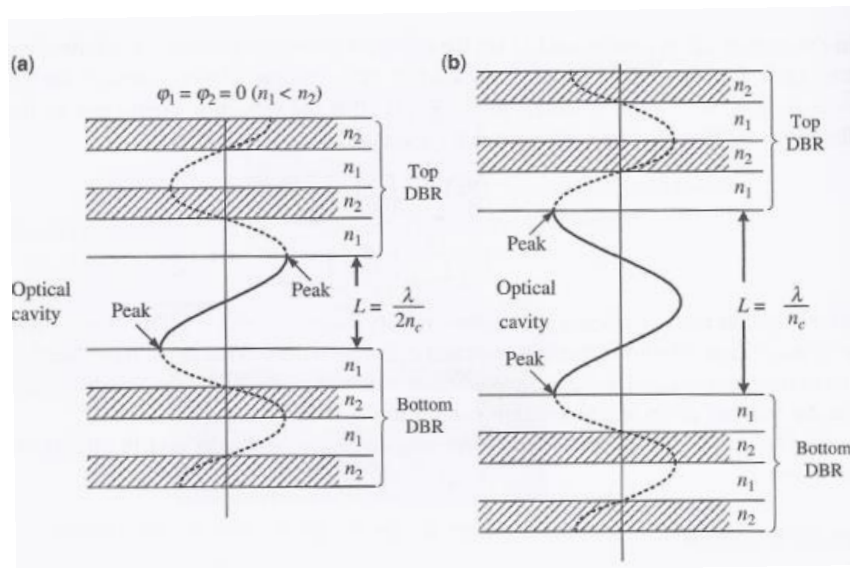
- ✓ **Constructive interference** between the incident and reflected waves
- ✓ Standing wave pattern will have a **peak** at the first interface of the top and bottom DBR

- ✓ **Destructive interference** between the incident and reflected waves
- ✓ Standing wave pattern will have a **null** at the first interface of the top and bottom DBR

# Surface Emitting Lasers

## ■ Design issues for active region II

- ✓ **Fabry-Perot (FP) MQW cavity** must satisfy resonance condition which occur when  $\beta L = m\pi$  ( $m=1,2,3\dots$ ) equivalently when the cavity length is an integral number of half wavelengths.



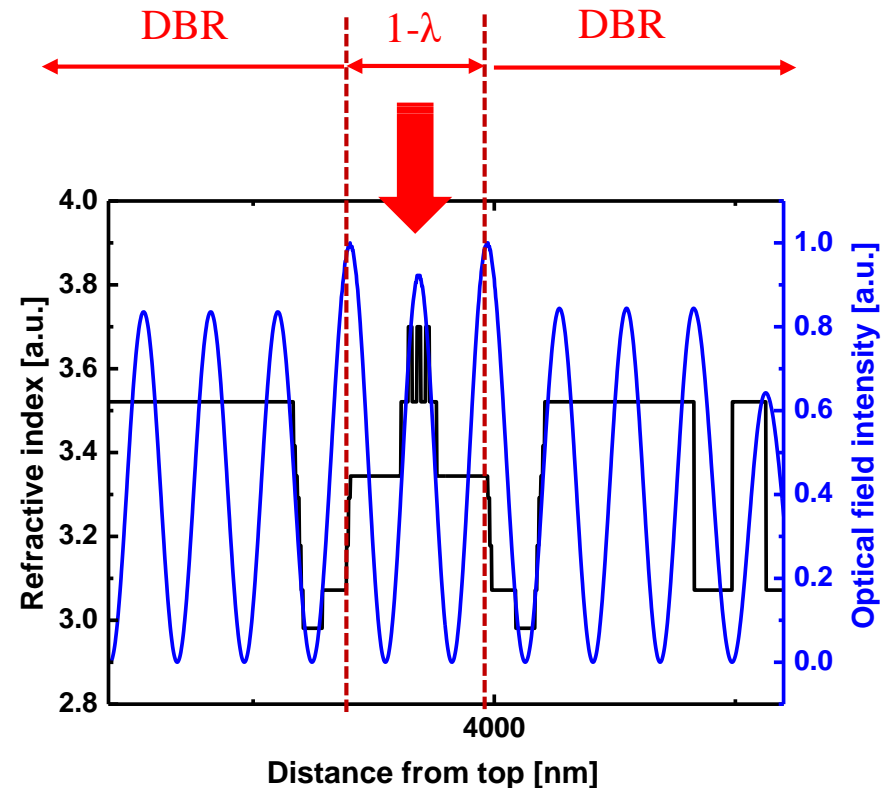
$$\beta L = m\pi$$

$$\therefore L = m \times \frac{\lambda}{2n} \quad m: \text{even number}$$


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**Resonance condition**

- ✓ For high efficiency laser, optical field is placed at quantum well region which occur when the cavity length is an integral *even number of half wavelengths*.



# Surface Emitting Lasers

## ■ Threshold condition

The threshold gain of a VCSEL is

$$\Gamma g = \alpha + \frac{1}{2L} \ln \left( \frac{1}{R_1 R_2} \right)$$

$\alpha$  : the optical absorptions inside and outside the active region,  
plus any diffraction loss

$\Gamma$  : the longitudinal and transverse optical confinement factor

Eq. (11.2.4)

where

$$R_1 = |r_1|^2$$

$$R_2 = |r_2|^2$$

$$\Gamma = \left( \gamma \frac{d}{L} \Gamma_t \right)$$

$d$  : the active layer thickness ,

$L$  : the cavity length

$\gamma$  : (1: thick active layer, 2: thin active layer) is placed at  
the maximum of the standing wave

$d/L$  : account for the longitudinal optical confinement

$\Gamma_t$  : the transverse optical confinement factor

Eq. (11.2.5)

Loss parameter

$$\alpha L = 2\alpha_i L_{eff} + 2\alpha_d L_{cavity}$$

$\alpha_i$  : absorption in DBR

$\alpha_d$  : diffraction loss due to the mode mismatch

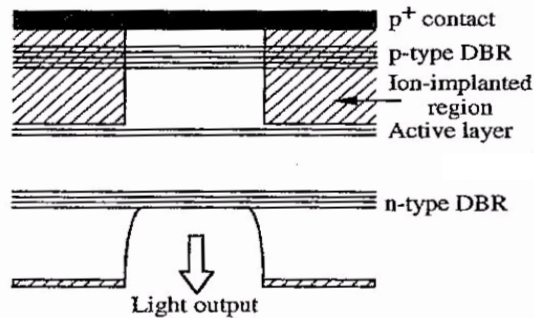
Eq. (11.2.6)

Depends on the size of the diameter of the active region and the locations of the mirrors.

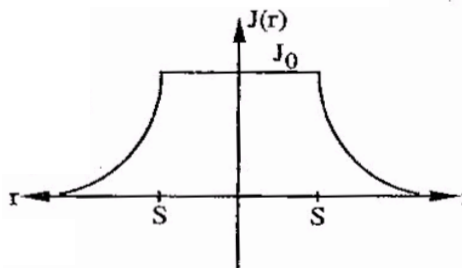
# Surface Emitting Lasers

## ■ Carrier injection and optical profile

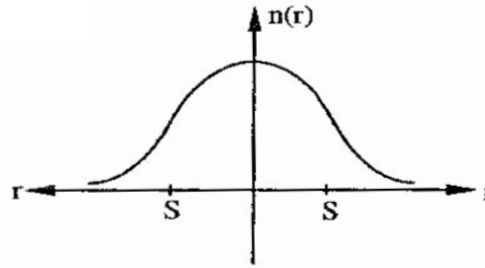
### Gain-guided VCSEL with ion-plantation region



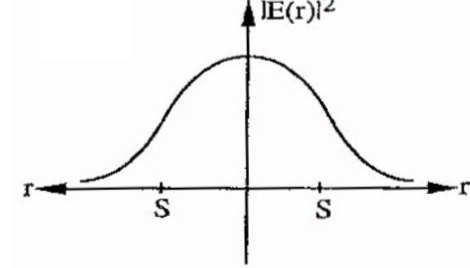
Current density



Carrier density



Fundamental optical mode profile

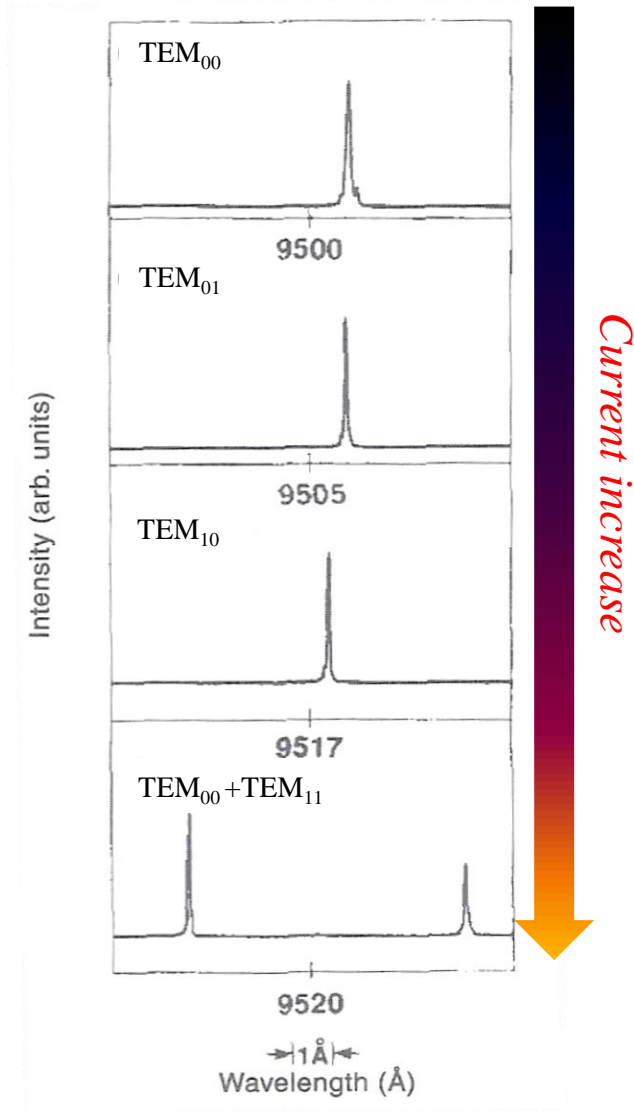
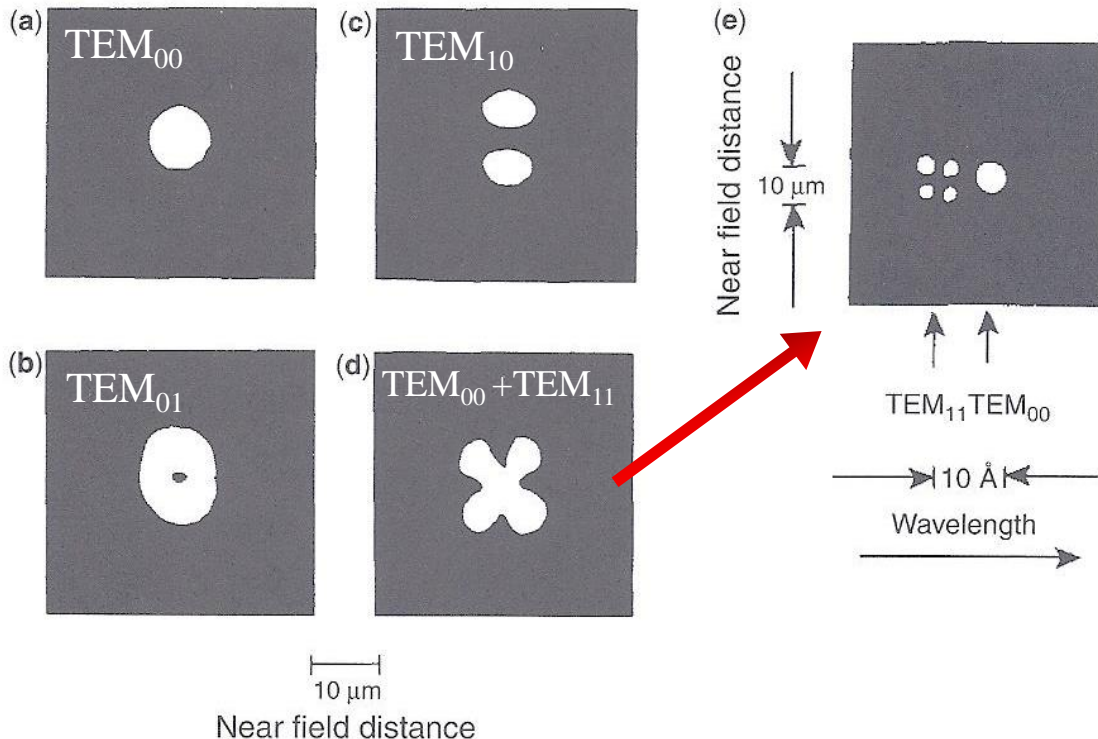


- ✓ Depending on the fabrication processes and the structures of the surface-emitting lasers, the *current distribution*, the *carrier density profile*, and the *optical mode pattern* vary.

# Surface Emitting Lasers

## ■ Intensity distribution of transverse modes

Near field patterns of a 15 $\mu$ m square VCSEL emitting

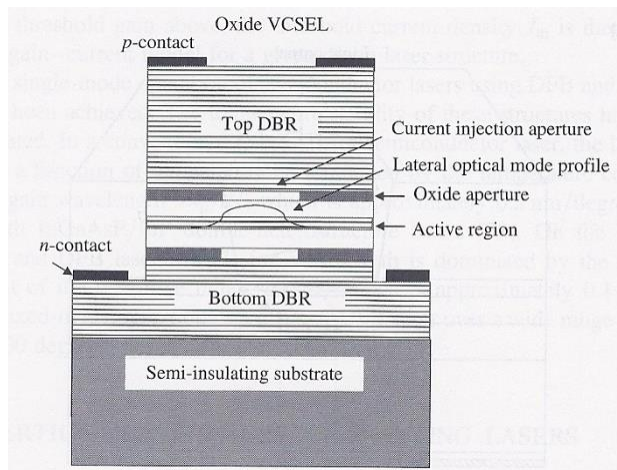


- ✓  $TEM_{00}$ ,  $TEM_{11}$  modes are clearly **separated** due to their **wavelength differences**.
- ✓ The **red shift** of the lasing wavelength is caused by the **junction heating** as the **injection current increases**.

# Surface Emitting Lasers

## ■ Oxide-VCSELs: Index Confinement

Lateral confinement by oxide-apertures forms apertures for current flow into the active region of the optical cavity. The lower refractive index of the oxide regions provides lateral index confinement of the optical mode.



< Double-aperture oxide confined VCSEL >

- Advantage of oxide-VCSEL
  - ✓ High power conversion
  - ✓ Low threshold current density
  - ✓ Low resistance design using parabolic hetero-interface grading
  - ✓ Minimize lateral current spreading
  - ✓ Lower refractive index provides index guidance and current flow

# Surface Emitting Lasers

## ■ Temperature Dependence and Junction Heating I

The junction heating is important in surface-emitting lasers.

A simplified mode for the temperature rise due to the injection current from a circular disk is

$$\Delta T_{jct} = \frac{P_{IV} - P_{opt}}{4\sigma S} \quad \text{Eq. (11.2.9)}$$

$P_{IV}$ : the total input electric power

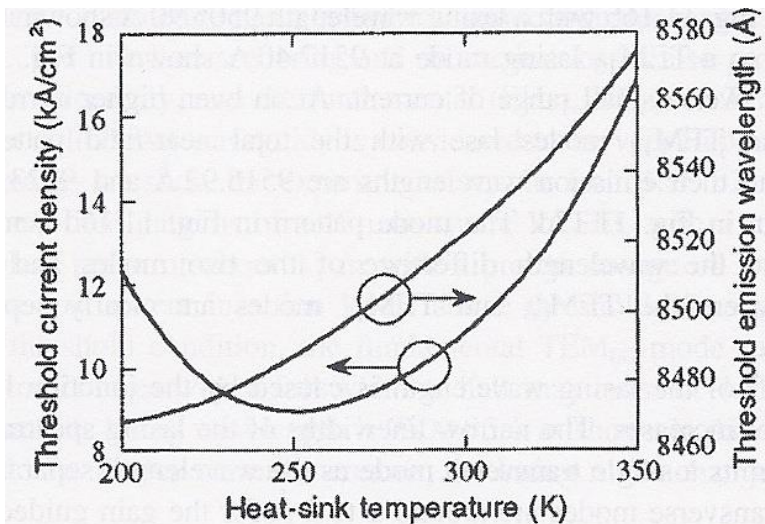
$P_{opt}$ : the optical output power

$\sigma$ : the thermal conductivity

$S$ : the disk radius

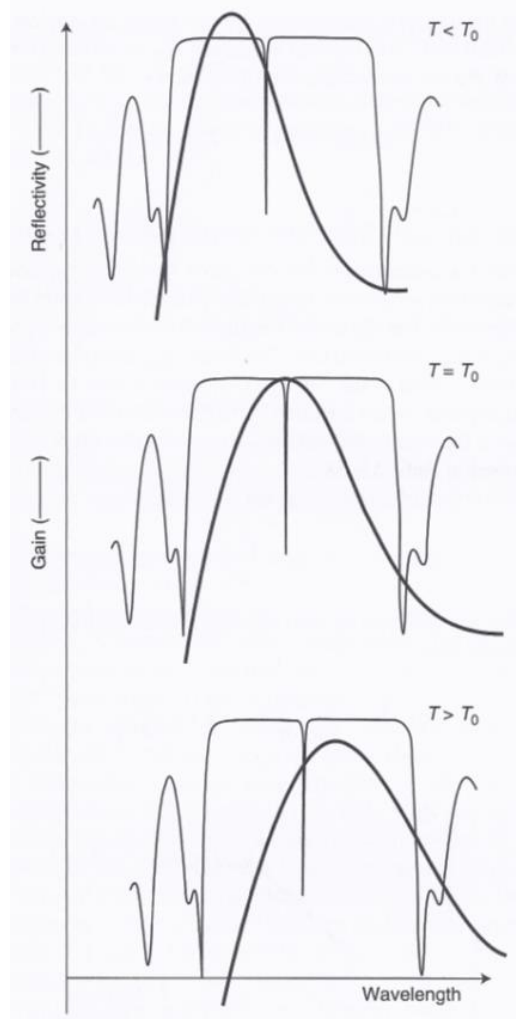
The dependence of the threshold current density and the emission wavelength as a function of the heat-sink temperature, based on a theoretical model.

For GaAs, the gain peak wavelength increase linearly at about 2.7 Å/K.



# Surface Emitting Lasers

## ■ Temperature Dependence and Junction Heating II



✓ Resonance  $\lambda$  / gain alignment

Temperature  $\uparrow$   $\rightarrow$  Bandgap and Index  $\uparrow$   
Optical length  $\uparrow$

- Long wavelength shift of resonance  $\lambda$  mode ( $0.8\text{\AA}/^\circ\text{C}$ )
- Long wavelength shift of gain peak ( $3.3\text{\AA}/^\circ\text{C}$ )

- ✓ Since Resonance  $\lambda$  shift toward long-wavelength faster than gain peak, gain peak must be placed lower than Resonance  $\lambda$ .
- ✓ The minimum threshold current ( $I_{th}$ ) occur when gain peak overlap Resonance  $\lambda$ .
- ✓ Threshold current ( $I_{th}$ ) increase as temperature goes up, resulting in degradation of performance of VCSEL.

# Surface Emitting Lasers

## ■ Optical Output and Differential Quantum Efficiency I

*The optical output power* is

$$P_{out} = \frac{\hbar\omega}{q} \eta [I - I_{th}(I, T_{jct})] \quad \text{Eq. (11.2.10)}$$

$$\eta = \eta_i \eta_{opt} \quad \text{Eq. (11.2.11)}$$

where  $\eta$  depends on two factors:

- (1) The **injection efficiency**( $\eta_i$ ) accounting for the fraction of injected carriers contributing to the emission process.
- (2) The **optical efficiency**( $\eta_{opt}$ ) accounting for the fraction of generated photons that are transmitted out of the cavity.

*The optical efficiency* is

$$\eta_{opt} = \frac{T_r}{A + T_r} \quad \text{Eq. (11.2.13)}$$

$$A = 2\alpha_i L_{eff} + \alpha_d L \quad T_r = \ln\left(\frac{1}{R_1 R_2}\right)$$

$A$ : the absorbance in top and bottom DBR

$L_{eff}$ : an effective penetration length

$L$ : the cavity length of the active layer

$T_r$ : mirror transmission loss

# Surface Emitting Lasers

## ■ Optical Output and Differential Quantum Efficiency II

*The power conversion efficiency* is given by

$$\eta_p = \frac{P_{out}}{VI} \quad \text{Eq. (11.2.14)}$$

$V$ : bias voltage

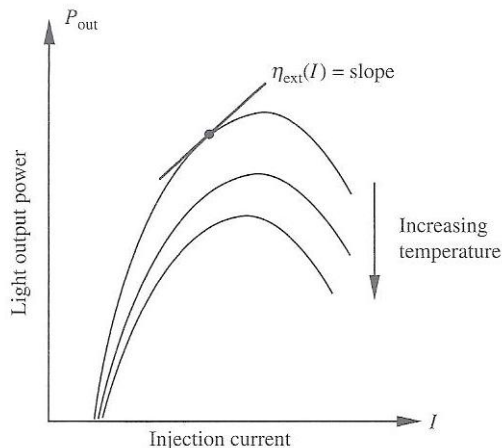
$I$ : bias current

$P_{out}$ : optical out power

*The differential quantum efficiency* is current-dependent

$$\eta_{ext}(I) = \frac{q}{\hbar\omega} \frac{dP_{out}}{dI} = \eta \left( 1 - \frac{dI_{th}}{dI} \right) \quad \text{Eq. (11.2.15)}$$

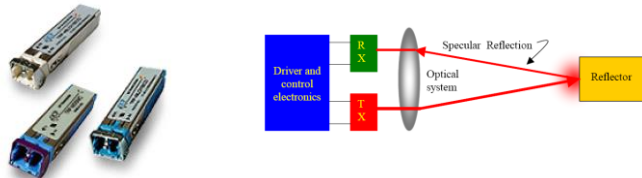


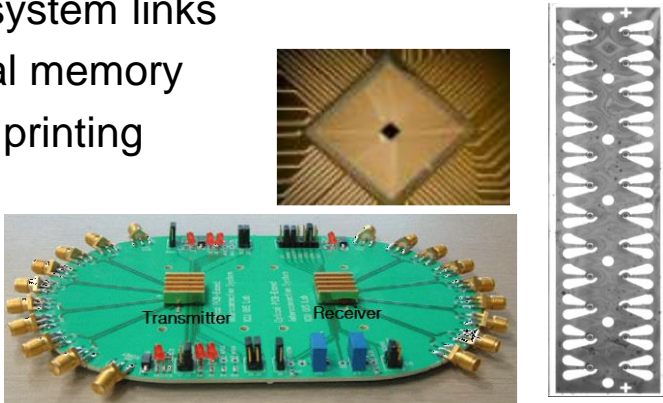
If  $dI_{th}/dI > 1$ , then the  $\eta_{ext}(I)$  can be negative as shown in figure.



A plot of the light output of a surface-emitting laser vs. the injection current for different temperatures. The slope at a particular current level  $I$  is the differential quantum efficiency, which can be negative at a high current level or a high temperature.

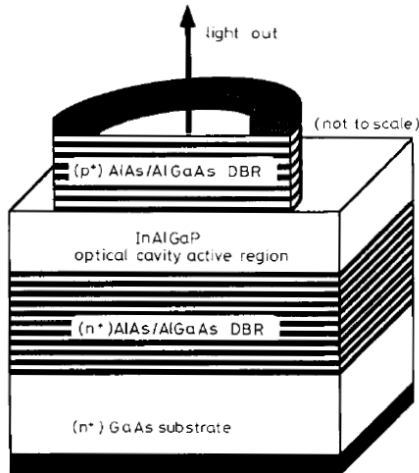
# Surface Emitting Lasers

## ■ Current and emerging VCSEL applications

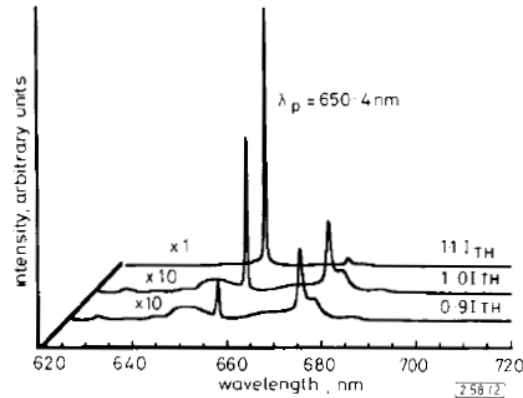
	Multi-mode operation	Single-mode operation
Single VCSEL	<ul style="list-style-type: none"> <li>Local area networks</li> <li>Storage area networks</li> <li>Bio-sensors</li> <li>Proximity sensors</li> </ul> 	<ul style="list-style-type: none"> <li>Laser absorption spectroscopy</li> <li>Chip-scale atomic clocks</li> <li>Laser based optical mouse sensors</li> </ul> 
Array VCSEL	<ul style="list-style-type: none"> <li>Very short reach (VSR) links</li> <li>Optical tweezers</li> <li>Optical pumping source</li> </ul> 	<ul style="list-style-type: none"> <li>Intra-system links</li> <li>Optical memory</li> <li>Laser printing</li> </ul> 

# Surface Emitting Lasers

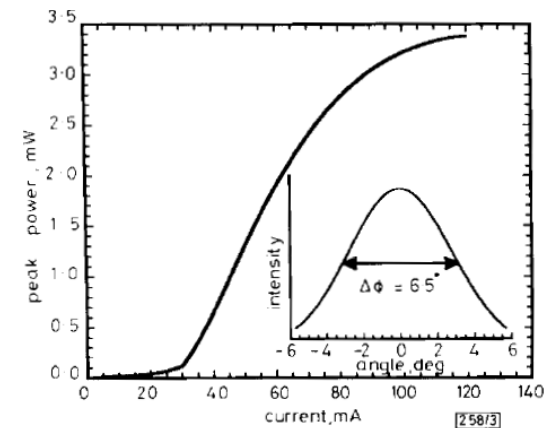
## ■ Red VCSELs



Visible VCSEL structure



Visible VCSEL lasing spectra



Light-current(LI) characteristic at room temperature

- Active layer: **InGaAlP/InGaAlP**
- In 1993, first demonstration of electrically injected visible VCSELs with an InAlGaP optical cavity active region\*.
- 630-670nm is considered as the laser for the **first-generation digital video disc system**.
- Sub-milliamper thresholds, 11% power conversion efficiency and 8mW output power have been achieved\*\*.
- Red VCSEL has been commercialized for **application to printers** and **plastic fiber communications**

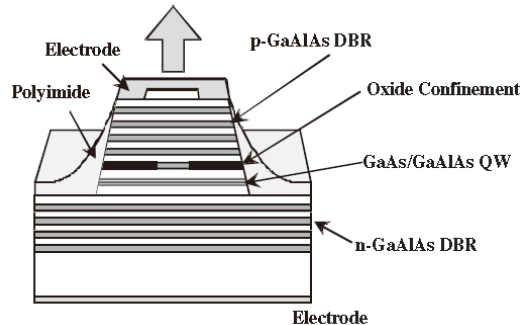
\*Lott, J.A. et al., "Electrically-injected visible (639-661nm) vertical cavity surface emitting lasers," *Electron. Lett.* 29, 830-832 (1993).

\*\*M. H. Crawford et al., *OSA Trends in Optics and Photonics Series*, Optical Society of America, Washington, D.C. 15, 104 (1998).

K. Iga, "Vertical-cavity surface-emitting laser: It's conception and evolution," *J. J. Appl. Phys.* 47, 1-10 (2008).

# Surface Emitting Lasers

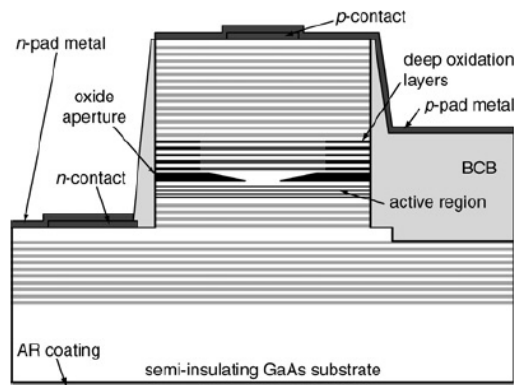
## ■ 850nm wavelength VCSELs



Typical structure of a 850nm GaAs-based VCSEL

- Active layer: **GaAs/AlGaAs**
- The first room-temperature CW operation was achieved in 1988.
- In production levels, **sub-mA thresholds and 10mW output** have been achieved.
- Wide temperature characteristics of 850 nm VCSEL is a candidate of a **light source of the media orientated system transport application\***.

## ■ 980nm wavelength VCSELs



High speed 980nm VCSEL

- Active layer: **InGaAs/GaAs/AlGaAs**
- In 1995, a novel laser structure employing a **selective oxidizing process** applied to AlAs.
- A relatively high power of more than 50mW may be possible.
- High-efficiency, high-speed, **tapered-oxide-apertured** 980 nm VCSELs with high data-rate/power-dissipation ratio of 3.5 Gps/mW, making these devices suitable for **interconnect applications\*\***.

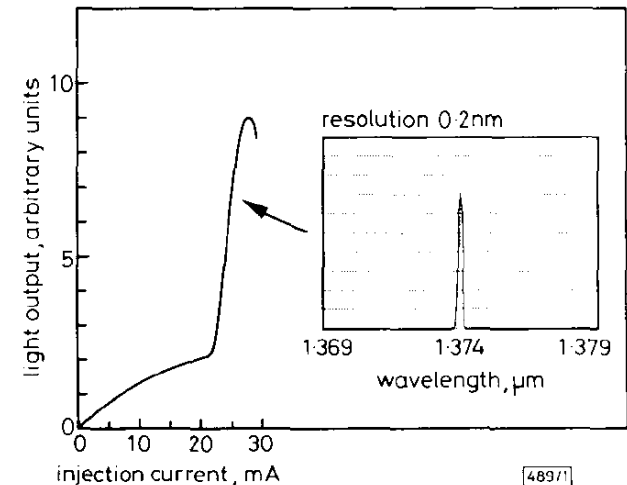
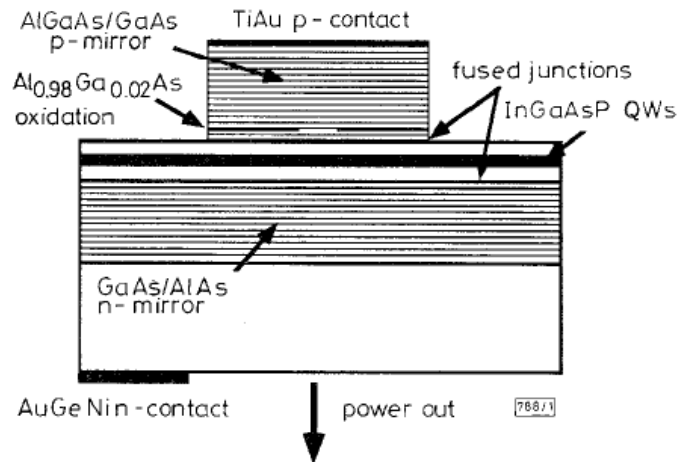
\*K. Nishikata. et al., "Wide temperature operation of 850nm VCSEL and isolator-free operation of 1300nm VCSEL for a variety of application," *Proc. of SPIE* 5737, 8-19 (2005).

\*\*Y. -C. Chang. et al., "High-efficiency, high-speed VCSELs with 35Gbit/s error-free operation," *Electron. Lett.* 43, 1022-1023 (2007).

K. Iga, "Vertical-cavity surface-emitting laser: It's conception and evolution," *J. J. Appl. Phys.* 47, 1-10 (2008).

# Surface Emitting Lasers

## ■ Long wavelength VCSELs on InP substrate



Epitaxial bonding of the InGaAsP/InP active region and GaAs/AlAs mirrors

CW operation for 1,300nm was demonstrated using MgO/Si mirror

- Active : **InGaAsP/InP**
- **Hybrid mirror technologies** are being developed since the index difference between InGaAsP and InP is too small.
- A **MgO/Si mirror** with good thermal conductivity was demonstrated to enable room-temperature CW operation for 1,300nm surface-emitting lasers for the first time\*.
- The CW threshold of 0.8mA and the maximum operating temperature of up to 71°C was reported for 1,550nm VCSELs with **double bonded mirrors**\*\*.
- **Parallel light wave systems** are necessary to satisfy the rapid increase in information transmission capacity in LANs.

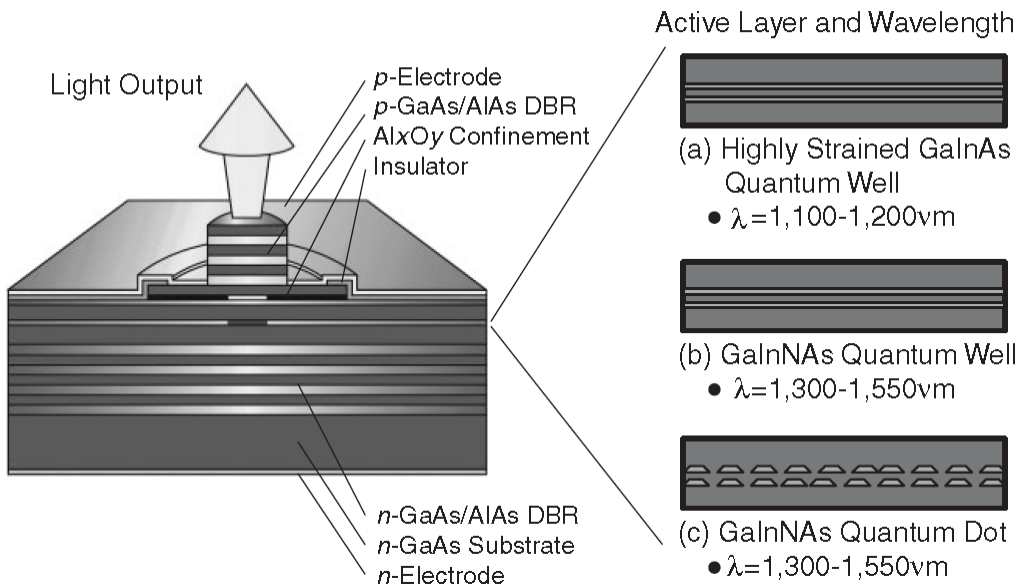
\* T. Bada, "Near room temperature continuous wave lasing characteristics of GaInAsP/InP surface emitting laser," *Electron. Lett.* 29 913-914 (1993).

\*\*N.M. Margalit et al., "Submilliamp long wavelength vertical cavity lasers," *Electron. Lett.* 32 1675-1677 (1996).

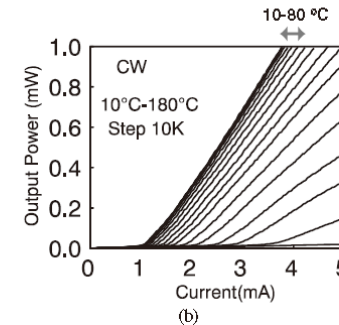
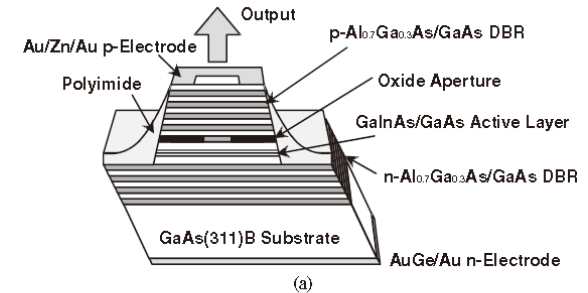
K. Iga, "Vertical-cavity surface-emitting laser: It's conception and evolution," *J. J. Appl. Phys.* 47, 1-10 (2008).

# Surface Emitting Lasers

## ■ Long wavelength VCSELs on GaAs substrate



Long wavelength VCSELs formable on GaAs substrate



Highly strained 1,200-wavelength GaInAs/GaAs VCSEL grown on (311)B substrate.

- Active layer: **InGaAsN/InGaAsN**, **InGaAsSb/GaAsN** and highly strained **InGaAs/GaAs/AlGaAs**
- GaAs/AlAs Bragg reflectors can be incorporated on same substrate.
- In content(=40%) can provide an excellent temperature characteristic.
- Viable for  $\lambda=1,200\text{nm}$  VCSELs for **silica-fiber-based high speed LANs\***.

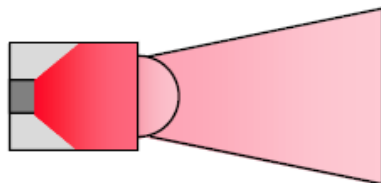
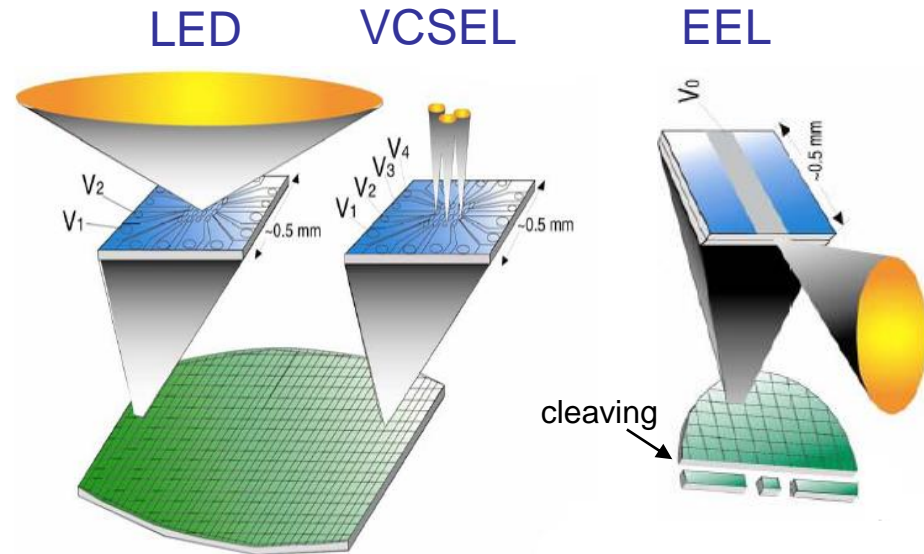
\*F. Koyama et al., "1.2um highly strained InGaAs/GaAs quantum well lasers for singlemode fiber datalink," *Electron. Lett.* 35 1079-1081 (1999).

K. Iga, "Vertical-cavity surface-emitting laser: It's conception and evolution," *J. J. Appl. Phys.* 47, 1-10 (2008).

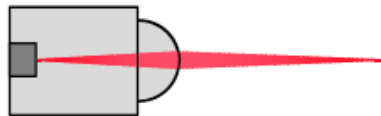
# Surface Emitting Lasers

## ■ VCSEL output beam properties

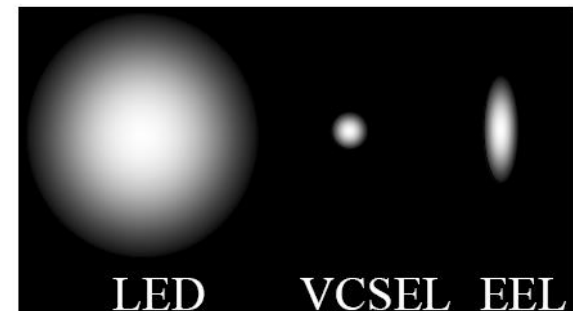
- Symmetrical beam
- Low divergence
- Simple, low cost optics



LED



VCSEL



LED

VCSEL

EEL

# Surface Emitting Lasers

## ■ Main parameters in VCSELs

Parameter	Symbol	Stripe Laser	Surface Emitting Laser
Active layer Thickness	$d$	100Å-0.1μm	80Å-0.5μm
Active Layer Area	$S$	$3 \times 300\mu\text{m}^2$	$5 \times 5 \mu\text{m}^2$
Active Volume	$V$	$60\mu\text{m}^3$	$0.07 \mu\text{m}^3$
Cavity Length	$L$	300μm	$\approx 1\mu\text{m}$
Reflectivity	$R_m$	0.3	0.99-0.999
Optical Confinement	$\xi$	$\approx 3\%$	$\approx 4\%$
Optical Confinement (Transverse)	$\xi_t$	3-5%	50-80%
Optical Confinement (Longitudinal)	$\xi_l$	50%	$2 \times 1\% \times 3$ (3QW's)
Photon Lifetime	$\tau_p$	$\approx 1 \text{ ps}$	$\approx 1 \text{ ps}$
Relaxation Frequency (Low Current Levels)	$f_r$	$< 5\text{GHz}$	$> 10\text{GHz}$

# Surface Emitting Lasers

## ■ High speed VCSELs

### • 3dB bandwidth in semiconductor lasers

$$f_{3dB} \cong \frac{\sqrt{1+\sqrt{2}}}{2\pi} \sqrt{\frac{v_g a}{qV_p} \eta_i (I - I_{th})}$$

$v_g$  : group velocity

$a$  : differential gain

$V_p$  : optical cavity volume

$\eta_i$  : internal quantum efficiency

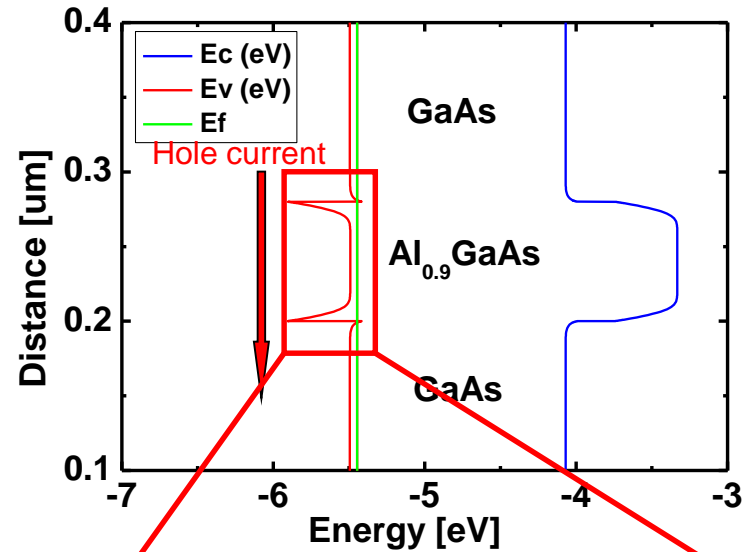
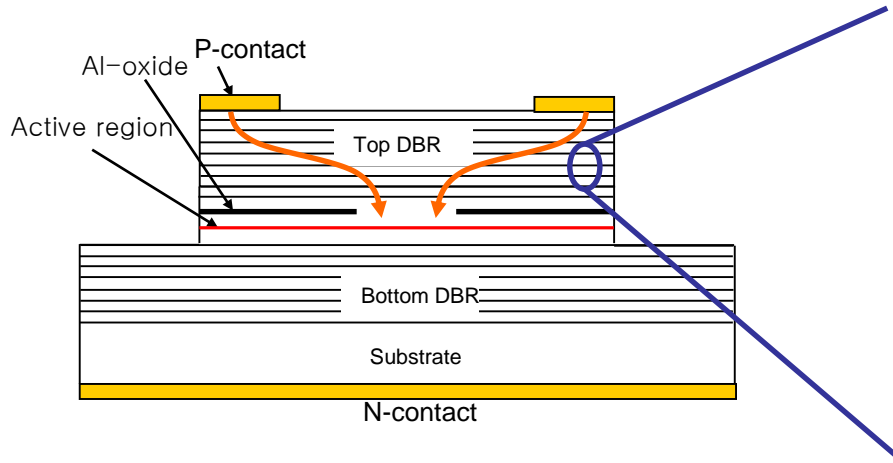
$I_{th}$  : threshold current

### To increase the modulation bandwidth

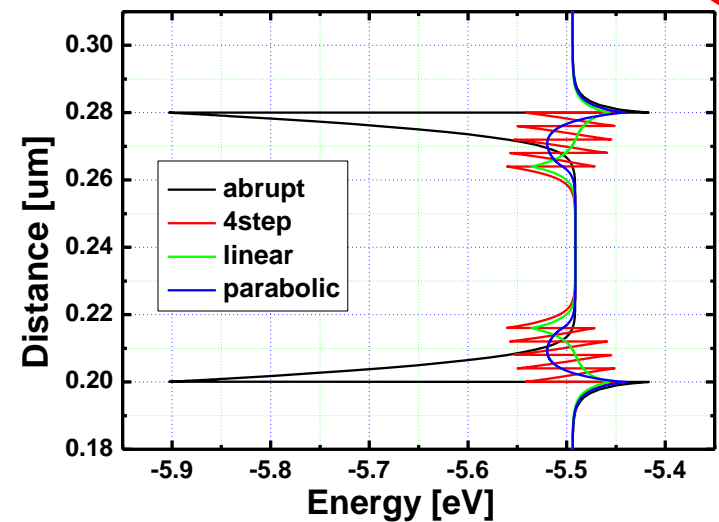
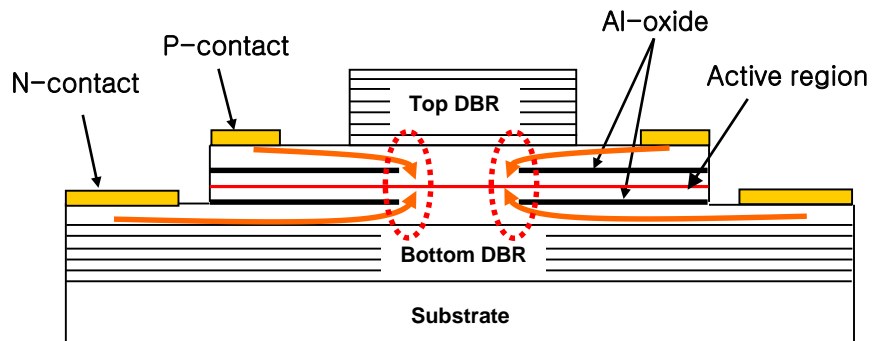
- ✓ Increase differential gain
  - Optimization the thickness and number of QW
- ✓ Decrease threshold current
  - Uniform carrier injection, Optimization of interface grading
- ✓ Decrease RC time constant
  - Coplanar contact, interface grading

# Surface Emitting Lasers

## ■ Extracavity contact

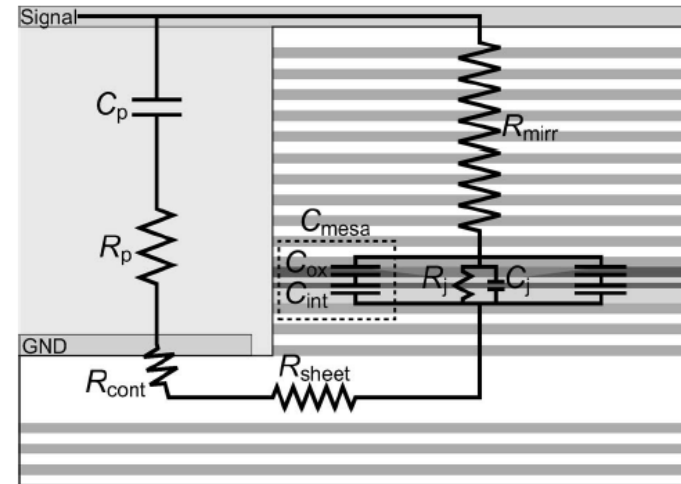
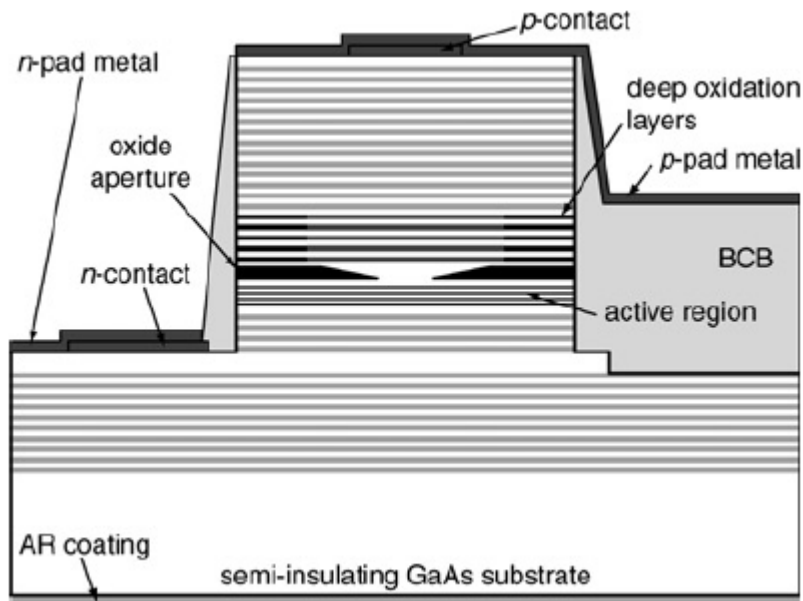


## ■ Intracavity contact

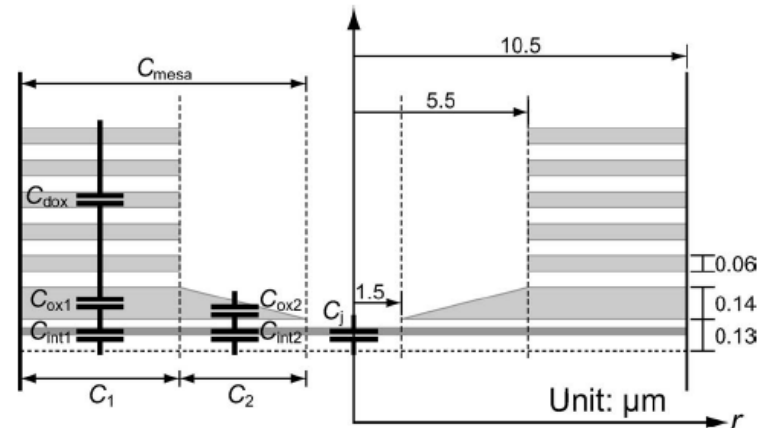


# Surface Emitting Lasers

## ■ High speed VCSELs



- Modified intra-cavity contact
- Tapered oxide aperture
- Deep oxidation layers

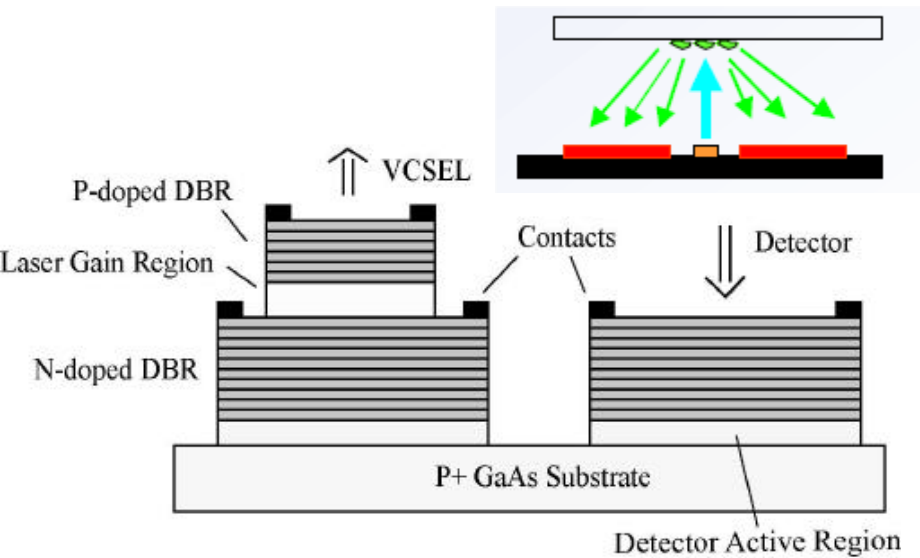


# Surface Emitting Lasers

## ■ VCSEL/PD integration

### VCSEL/pin-PD integration

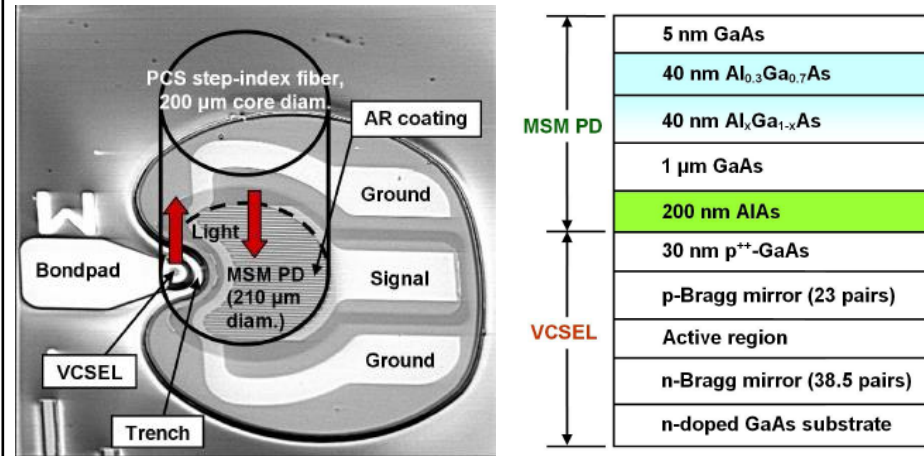
(Stanford Univ., 2004)



- ✓ VCSEL/pin-PD integration for bio sensor application
- ✓ Not applicable to high-speed operation

### VCSEL/MSM-PD integration

(Univ. of Ulm, 2003)



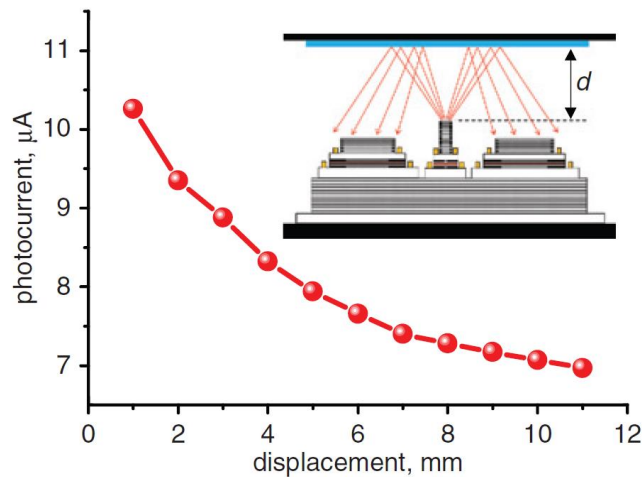
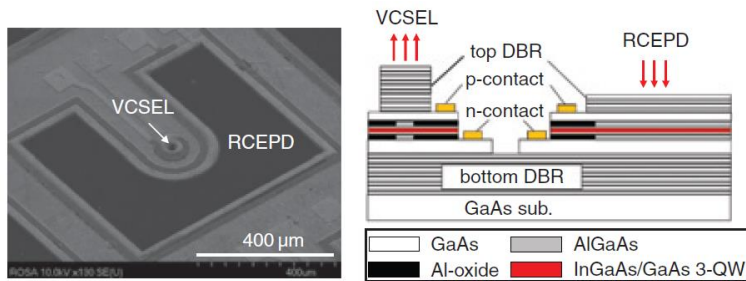
- ✓ VCSEL/MSM-PD integration for transceiver application
- ✓ Bi-directional optical interconnects

# Surface Emitting Lasers

## VCSEL/PD integration

### VCSEL/RCEPD integration

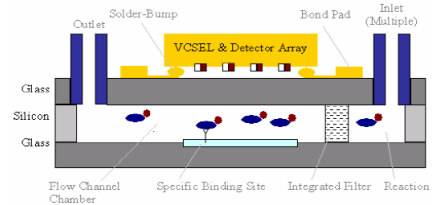
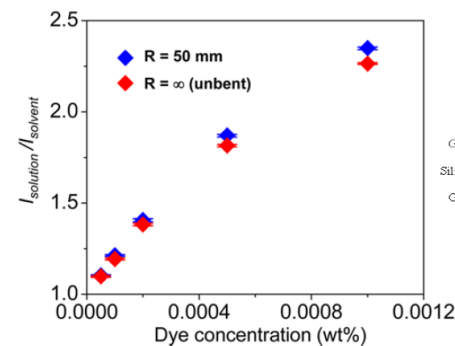
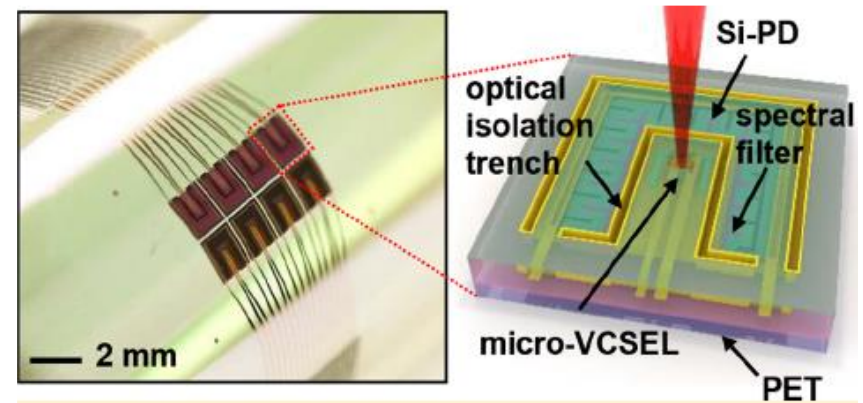
(GIST, 2016)



- ✓ Monolithic integration
- ✓ Displacement sensor applications

### VCSEL/ Si-PD integration

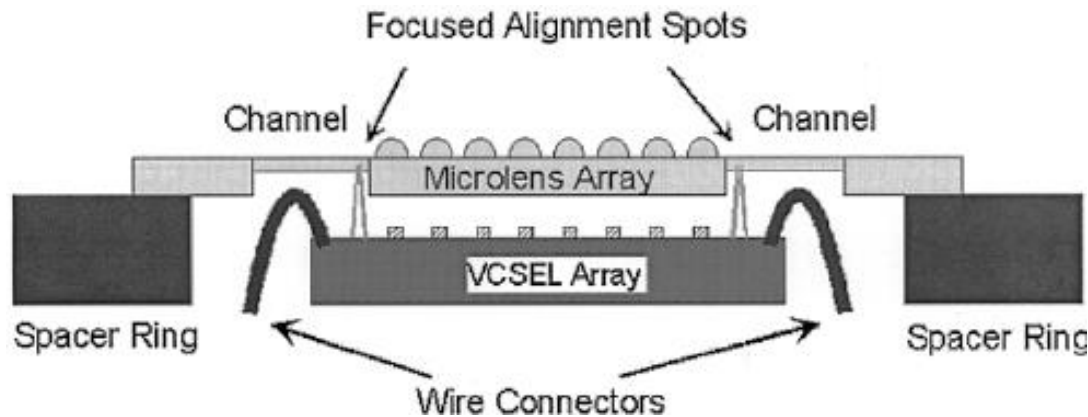
(USC, 2016)



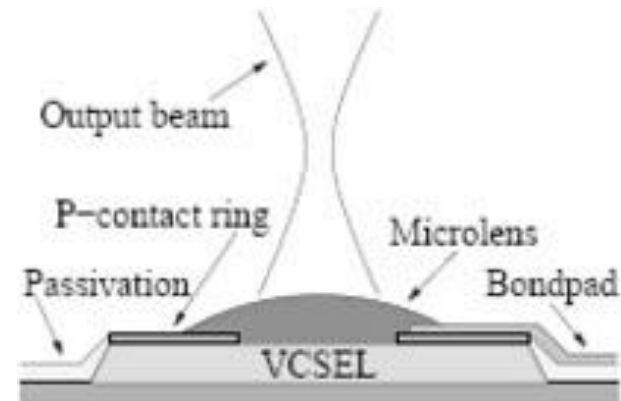
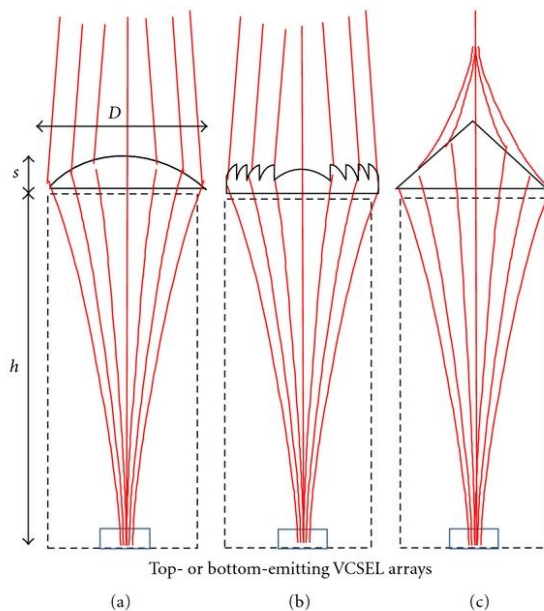
- ✓ Hybrid integration
- ✓ Flexible forms, optofluidic applications

# Surface Emitting Lasers

## VCSEL – microlens integration



✓ 2D VCSEL arrays for optical interconnects

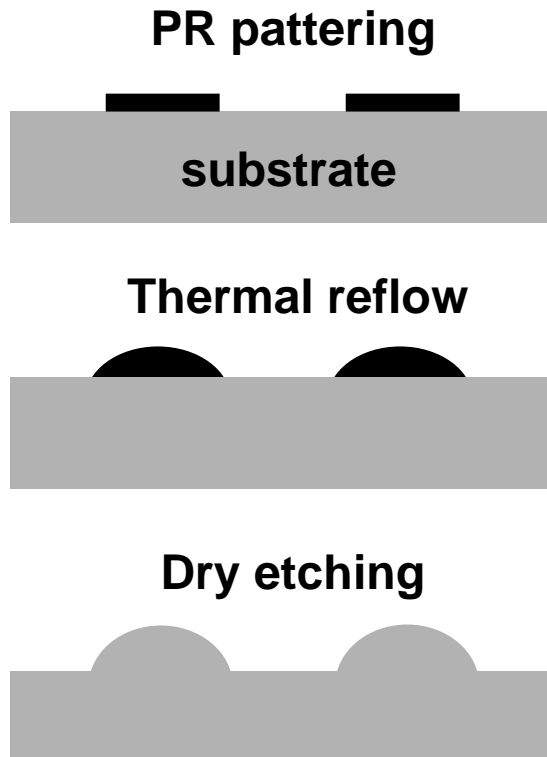


✓ Volume reduction  
✓ Beam shaping

# Surface Emitting Lasers

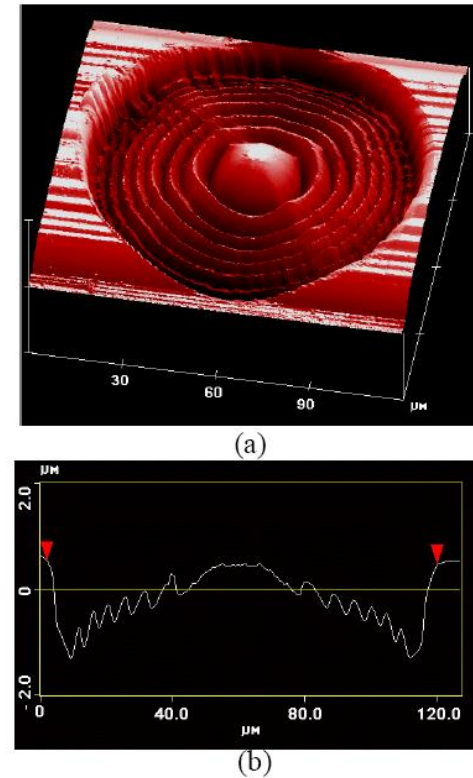
## ■ VCSEL – microlens integration

### PR reflow + dry etching



E. M. Stzelecka et al., Microelectron. Eng. 35, 385 (1997)

### Focused ion beam milling



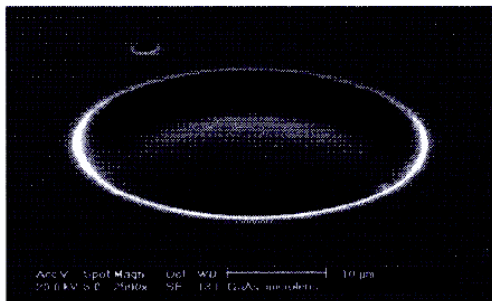
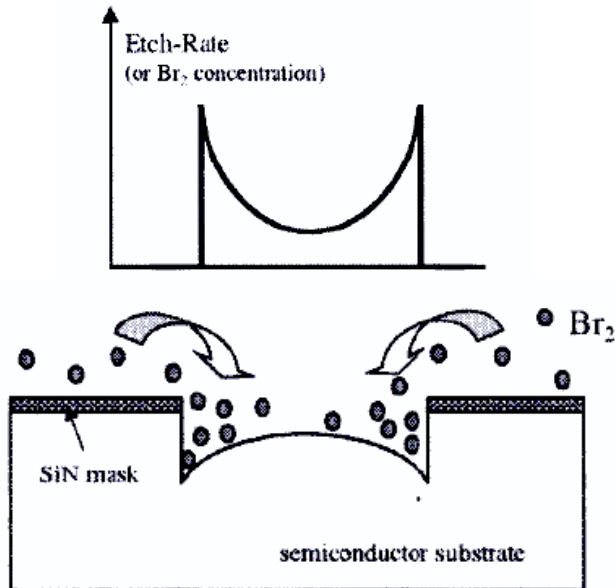
F. Qi et al., Opt. Express 10, 413 (2002)

# Surface Emitting Lasers

## ■ VCSEL – microlens integration

### Diffusion-limited wet-etching

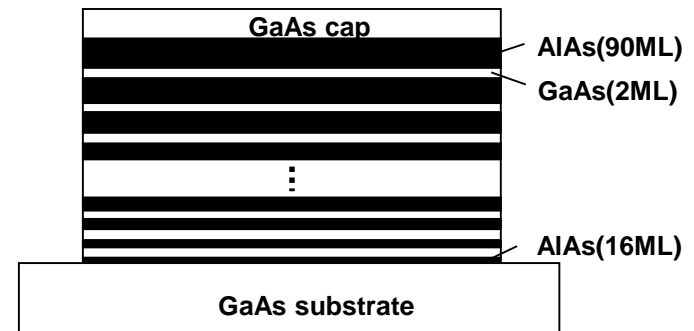
(SNU, 2000)



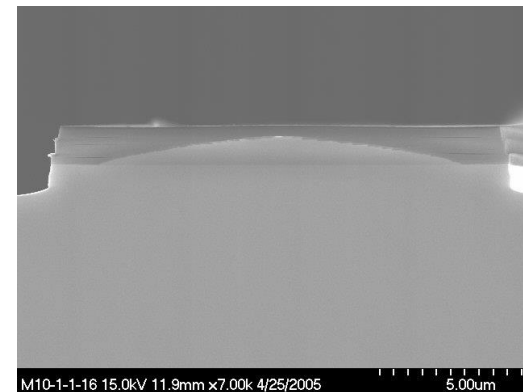
### Selective oxidation

(GIST, 2006)

#### Epitaxial layer structure



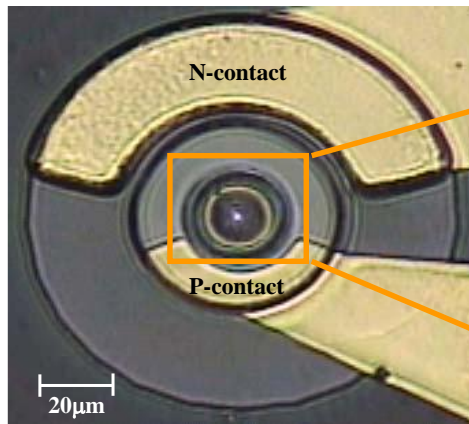
Linear composition grading of Al<sub>x</sub>Ga<sub>1-x</sub>As (x=0.89~0.98) using **digital alloy** method



# Surface Emitting Lasers

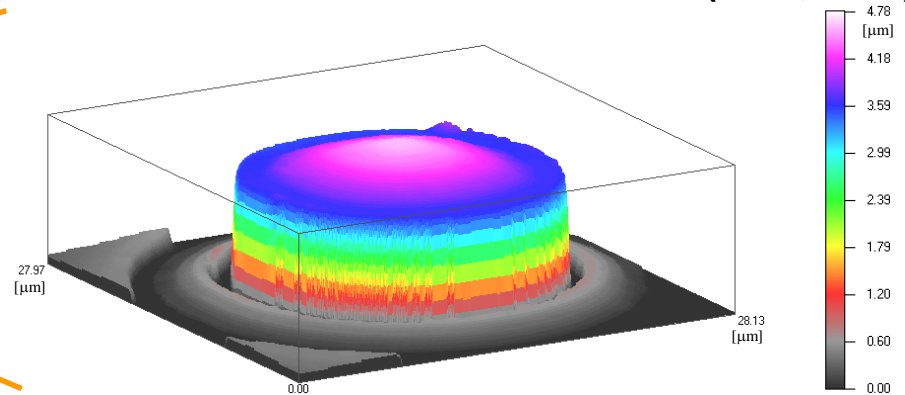
## ■ VCSEL – microlens integration

### Optical microscope image

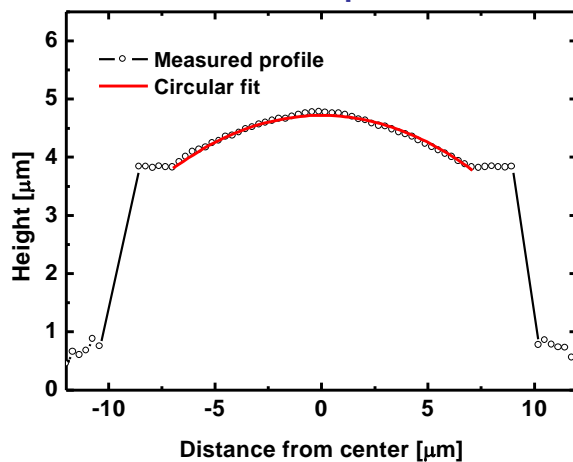


### 3-D confocal microscope image

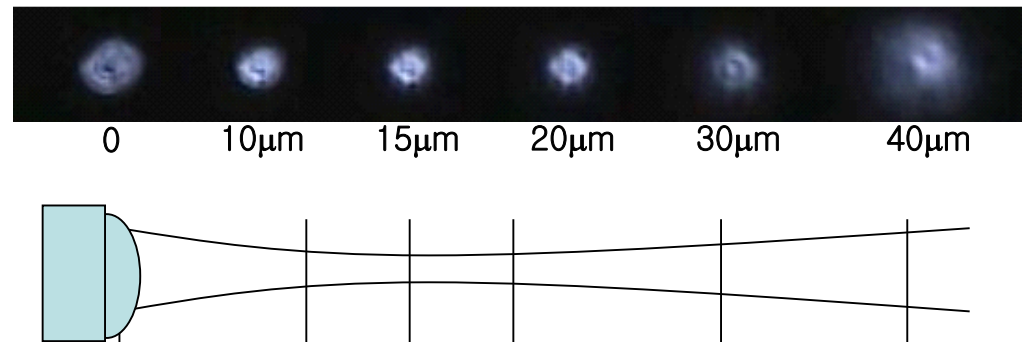
(GIST, 2007)



### Microlens profile



### Output beam from oxide-removed microlens-integrated VCSEL



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**Question or Comment?**